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**OBSERVATORIO ASTRONOMICO NACIONAL
BIBLIOTECA - ENSENADA**

INSTRUCTION MANUAL

CASSEGRAIN SPECTROGRAPH

For

OBSERVATORIO ASTRONOMICO DI BRERA

JOB 59007

July 1975

Prepared by

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PREFACE

This instruction manual is for the Cassegrain Spectrograph manufactured by Boller & Chivens for the Observatorio Astronomico di Brera. The Spectrograph is to be used at the f/7 Cassegrain focus of the 1.37M telescope. This manual provides a brief description of the component parts of the spectrograph, together with their function, alignment and adjustment procedures, and general information on the use of the spectrograph.

1.0 DESCRIPTION OF THE SPECTROGRAPH (Ref. Drawing E-43488)

A description of the functioning parts and assemblies of the spectrograph is necessary to provide the operator with a complete knowledge of the features and proper operation of the spectrograph. This section of the manual should be read carefully before attempting to use the instrument. In most cases, reference should also be made to the assembly and sub-assembly drawings furnished separately from this manual. These drawings include complete parts lists for commercial and special manufactured parts, and will prove invaluable if any maintenance work is required.

Light passes from the telescope through the slit and is collimated by an off-axis parabolic mirror. The collimated light is dispersed by a diffraction grating and is then reimaged by the camera onto the photographic plate. Other features include a decker, filter holder, provisions for an exposure meter, shutter, comparison light system, a 14 cm direct photography camera, and a 45 cm direct photography camera. Drawings E-43488 and D-43800 show the exterior configuration of the spectrograph and the optical diagram.

The spectrograph is basically light-tight and need not be operated in total darkness. If the spectrograph is tested off of the telescope, precautions must be taken to prevent outside light from entering the opening at the upper end.

In very brief form, the operating procedures would be as follows:

- a. With the spectrograph mounted on the telescope, set the desired grating angle, slit and decker positions, filter, and collimator focus.
- b. With the viewing periscope in the upper position and the comparison periscope knob in the "OUT" position, guide the telescope to position a star on the slit.
- c. With the shutter closed, place a loaded plateholder in the camera, ready for starting an exposure. (Note that the red light is on when the shutter is closed). Open the dark slide of the plateholder.
- d. To produce a portion of the comparison spectra exposure, select the source desired, push the comparison periscope knob to the "IN" position, start the source and open the shutter for the desired length of time.
- e. Open the shutter to start the stellar exposure and operate the telescope controls as necessary to drift the star along the slit.
- f. The comparison sequence, part d, should be repeated at the middle and end of the stellar exposure.

The basic procedure for checking alignment of the spectrograph and of the collimator mirror is as follows:

- a. Image a point source of light at the center of the slit so that the axis of the point source is normal to the face of the spectrograph mounting flange. Or, place a standard 15 watt bulb in the Neon comparison system.

- b. Remove the collimator assembly (item 19 on Drawing E-35093) and place a piece of vellum over the end of the collimator tube. Check to see that the illuminated area is uniform, centered, and 3.5 to 4.0 inches in diameter.

- c. With the camera removed, and either the grating or a plane mirror in the grating holder and set near zero, observe the illuminated area of the grating or mirror. Also, rotate the grating in a positive direction and note the extremes of the illuminated area in the direction of dispersion. In either case, if the illuminated area is not symmetrical with the area of the grating face, the collimator mirror should be readjusted. (See Section 2.1).

More detailed instructions for the alignment of the spectrograph are contained in Section 2.0 of this manual.

1.1 FOCAL RATIO CONVERTER (Ref. Drawing C-44614)

1.2 COMPARISON SPECTRUM SYSTEM (Ref. Drawings C-27892,
C-35092, and C-44900)

A comparison light source is included in the spectrograph for use in identifying the wavelength of lines on the photographed spectrum. The comparison spectrum system consists of two light sources, an Iron-Argon hollow cathode and a Neon bulb, and a periscope assembly which can inject the comparison source into the light path of the spectrograph when a comparison spectrum is to be photographed.

The neon light source is mounted on one side of the spectrograph and the hollow cathode on the opposite side. The neon source uses a NE-40 neon glow bulb and can be turned on and off by a switch mounted in the same housing as the neon bulb. Attached on the outside of the neon light source housing is a milky white translucent bulb. When the neon source is on, a faint glow is detectable through this bulb.

The hollow cathode tube is argon filled and has an iron cathode. The tube is a Westinghouse WL22611. To change tubes, take off the end cap (part B-35831), unplug the tube, and pull it out.

The light from either comparison source is projected onto the slit through the periscope assembly. The periscope assembly must be pushed in before the comparison light is projected onto the slit. Note that stellar light is blocked from the slit when the comparison periscope is in the "IN" position. The outer knob of the periscope has an engraved arrow which should be turned toward the hollow cathode source when this is used and toward the neon source when this is to be used.

1.3 SLIT AND DECKER ASSEMBLY (Ref. Drawing D-39013)

Light from a star which is focussed by the telescope will converge to a focus at the front surface of the slit jaws inside the spectrograph. The slit assembly consists of two ^{3.81 cm} 1-1/2 inch long polished and aluminized jaws. This is a biparting slit and the jaws are continuously adjustable over a range from 5 to 1200 microns. Both jaws move in the direction of the slit length for changes in slit width. The jaws remain parallel up to a slit opening of approximately 500 microns. For larger openings, some tapering of the slit will be noticed. This is due to a special flexure arrangement used in the control mechanism and is not considered serious, as wider slit widths are normally used only for certain test purposes.

The slit width is set by the slit micrometer. This micrometer reads the slit width directly in microns. The slit assembly has been adjusted so the minimum width will remain at 5 microns, even though the micrometer is adjusted to zero. The slit jaws have been adjusted for parallelism to an accuracy of ± 1 micron. A knurled ring at the base of the micrometer barrel is a lock and when rotated fully clockwise locks the micrometer barrel against accidental rotation. To release the lock, turn the knurled ring to the full counterclockwise position.

To clean the slit jaws, use of an electrostatic brush or a very soft camel hair brush is recommended. Harder objects should not be placed against the sharp edge of the slit jaws, as these edges are very fragile.

The decker adjustment which is part of the slit assembly consists of a mask-template device placed over the slit jaws. This mask is movable in a direction perpendicular to the slit length and is controlled by a rotating dial located at the outside end of the unit. Rotation of the dial selects any of the slit length combinations indicated in Table 1 and Table 2.

TABLE 1

14 cm CAMERA

0.222

16
Fomation
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reson vehicles

Position

Comparison Window

Projected Inner
Dimension with
14 cm FL Camera

Projected Outer
Dimension with
14 cm FL Camera

#1 - 2 mm windows,
separated by 2 mm

0.44 mm

1.33 mm

#2 - 2 mm windows,
separated by 3 mm

0.67 mm

1.56 mm

#3 - 2 mm windows,
separated by 5 mm

1.11 mm

2.00 mm

#4 - 3.5 mm windows,
separated by 10 mm

2.22 mm

3.78 mm

#5 - 3.5 mm windows,
separated by 18 mm

4.00 mm

5.55 mm

Stellar Windows

#1 - 1 mm window

0.22 mm

12.9

#2 - 2 mm window

0.44 mm

74.9

#3 - 4 mm window

0.89 mm

51.6

#4 - 8 mm window

1.78 mm

123.6

#5 - 16 mm window

3.55 mm

226.4

#6 - 25 mm window

5.55 mm

322.5

Wedge Window

Width of wedge is variable from 0 to 2.54 mm.

TABLE 2

45 cm CAMERA

<u>Position</u>	<u>Projected Inner Dimension with 45 cm FL Camera</u>	<u>Projected Outer Dimension with 45 cm FL Camera</u>
<u>Comparison Window</u>		
#1 - 2 mm windows, separated by 2 mm	1.43 mm	4.29 mm
#2 - 2 mm windows separated by 3 mm	2.14 mm	5.00 mm
#3 - 2 mm windows, separated by 5 mm	3.57 mm	6.43 mm
#4 - 3.5 mm windows, separated by 10 mm	7.14 mm	12.14 mm
#5 - 3.5 mm windows, separated by 18 mm	12.86 mm	17.86 mm
<u>Stellar Windows</u>		
#1 - 1 mm window		0.71 mm
#2 - 2 mm window		1.43 mm
#3 - 4 mm window		2.86 mm
#4 - 8 mm window		5.71 mm
#5 - 16 mm window		11.43 mm
#6 - 25 mm window		17.86 mm

Wedge Window

Width of wedge is variable from 0 to 2.54 mm.

The entire slit assembly may be removed from the spectrograph by first removing three cap screws on the outside flange, just outside of the decker dial. After removing the screws, carefully remove the slit assembly from the spectrograph. It may be necessary to rotate the decker dial to put the decker in a proper position for clearing the spectrograph body.

1.4 SLIT VIEWER (Ref. Drawing D-41010 and C-41036)

Included on the spectrograph is a two-position periscope, normally used for guiding the telescope by observing reflected starlight off of the aluminized slit jaws. The periscope may be rotated from the normal position, which permits viewing the upper face of the slit jaws, to the lower position which permits viewing a star through the slit. This is accomplished by rotating the assembly by 180° using the handle, part A-41024. Note that the periscope rotates through only one 180° sector.

The periscope assembly consists of a pick-up mirror, a pair of symmetrical achromatic lenses, a second diagonal mirror, and a wide-field Clave' eyepiece. The pick-up mirror, part A-41018, for viewing the reflected light off the slit jaws is mounted to the inside of the spectrograph flange. The turning mirror, part A-41040, for viewing through the slit is part of the Filter-Mirror Subassembly (C-41036). The eyepiece can be slid in and out to permit fine focus adjustment by loosening the clamp ring, part B-41013, and the entire right angle assembly can be rotated 360° by loosening the other clamp ring (B-41013). Note that when viewing starlight through the slit, that all light from the slit to the collimator mirror and the rest of the spectrograph is blocked.

1.5 FILTER-MIRROR SUBASSEMBLY (Ref. Drawing C-41036)

This subassembly is shown on Drawing C-41036. It can be rotated to three different positions:

1. "MIRROR" which sends the light coming through the slit to the slit viewer. When it is in this position all the light to the collimator is blocked.
2. "FILTER" if desired, a filter (.49-inch x 1.62-inch x .25 inch thick) can be mounted in its cell. To change filters, remove the entire subassembly from the spectrograph (take out the three mounting screws, item 7), remove the clips (parts A-41042-1 and -2), and place the filter in position. If a thinner filter is desired, shims can be made to make the 0.25-inch total thickness.
3. "CLEAR" this position can be used when a filter is mounted and it is desired to take a spectra without the filter in the light beam.

1.6 SHUTTER (Ref. Drawing D-26703)

A shutter is located along the optical axis between the slit and the collimator mirror. This shutter is used to cut off all light to the interior of the spectrograph when the camera is being loaded. To remove the light shutter from the light path, pull the knob found on the slit side of the spectrograph. A red warning light on the shutter assembly remains off when the spectrograph power is turned on and when the shutter is out of the light beam. The light off thus indicates that the shutter is open.

1.9 GRATING ASSEMBLY (Ref. Drawing D-43671)

The entire grating assembly is removable as a unit assembly from the side of the spectrograph. It must be removed for exchanging gratings. To remove it, first remove the four cap screws holding it in the housing, and then gently pull the grating assembly out, using the two handles. Rods inside the spectrograph guide the assembly in and out to protect the grating from damage during removal. Extreme care should be taken in removing the grating assembly, not to place hands or fingers on the surface of the diffraction grating. In replacing the grating assembly, note that there is a slot in one side of the outer flange which must line up with a fixed pin in the spectrograph body.

The grating assembly permits rotating the grating through a range of angles from normal to the collimator beam (-25°) to +60°. The least division on the dial vernier is 5 arc minutes. The position for auto-collimating the collimator beam back to the slit is approximately -25°. Note that there is a + sign engraved on the grating dial and the grating is installed such that the grating angle is positive. Table 3 gives the grating angle for the grating furnished. A lock mounted on the outside of the grating dial locks the grating firmly.

The interchangeable grating cells are held in place by four screws, one at each corner of the cell. Before removing or replacing a grating cell, the plastic cover which is provided for each grating cell should be put in place. Extreme care should be taken to place the plastic cover down, parallel to the face of the gratings, so that there is no possibility of the cover contacting the grating. In installing the grating cell, the engraved arrow on the side of the cell should point to the right when you are standing facing the dial end of the assembly.

One grating was supplied. The grating information is listed in Table 3.

1.7 EXPOSURE METER (Ref. Drawing D-38986)

Only the optical and mounting equipment has been furnished. The exposure meter tube and housing can be easily added later. A small mirror on a push rod is located on the same side of the spectrograph as the slit assembly. When this rod is pushed in, a small 45-degree diagonal mirror is inserted in the forward edge of the collimated beam, and deflects a small amount of the light at right angles to the exposure meter photomultiplier tube mounted on the opposite side of the housing. The mirror was adjusted during alignment and was aimed so that the field lens just forward of the photomultiplier housing imaged the mirror itself on the face of the photomultiplier tube. Note that the image of the mirror on the photomultiplier tube is elliptical.

1.8 f/7 COLLIMATOR (Ref. Drawing E-35093)

The collimator located at the bottom of the spectrograph is an f/7 off-axis portion of a parabolic mirror. This mirror produces a collimated beam on an axis of approximately 9 degrees toward the grating and camera side of the spectrograph. The mirror has a clear aperture of 100mm, although the diameter of an f/7 beam from the slit is 90mm.

The collimator mirror mount provides a focus travel of ± 0.75 inches from a nominal position. A dial indicator is provided which reads in 0.001 inch increments, so that each unit of the indicator represents $25\mu\text{m}$ of motion of the collimator mirror. The extreme focus position corresponds to a reading of zero (farthest from the slit), and a reading of 1.500 (for the mirror in the closest position).

Extreme care must be taken in handling and cleaning the mirror, since the surface is aluminized but not overcoated.

TABLE 3

Camera	Grating	Order	Grating Angle	Centered Wavelength Å	Dispersion Å/mm
14 cm FL	600 l/mm 5000Å	1st	+8° - 38'	4550	114
45 cm FL	600 l/mm 5000Å	1st	+8° - 38'	4550	35

1.10 14 cm DIRECT PHOTOGRAPHY CAMERA (Ref. Drawing D-42440)

This camera consists of the Bowen Optics Module (D-35089) and parts D-40839 (Direct Photo Housing), D-35480 (Lens Holder), and A-35448 (Field Flattener - 'Thick'). The field flattener is epoxied into the lens holder and the lens holder attaches to the direct photo housing by means of three sets of push-pulls. The field flattener was adjusted with the push-pull screws to place it coincident with the focal plane and to take out any tilt in the focal plane.

1.10.1 Schmidt Camera Assembly (Ref. Drawing D-35089)

The camera optics were designed by Dr. Ira Bowen. The optics were aligned at Boller & Chivens. This alignment included centering of the corrector plate with respect to the solid block (using set screws, item 7 on subassembly drawing D-35089) and spacing of corrector with respect to the solid block (using item 2 on subassembly drawing D-35089). The reflective coating on the two surfaces of the solid block is aluminum. The corrector plate and solid block are fused silica with no overcoating.

1.10.2 Plate Holders (Ref. Drawing D-40841)

Two plate holders have been supplied with the spectrograph. To install the plate holder in the camera, place the plate holder in position in part C-35021, subassembly D-40838, turn the clamping retainers (part A-35034, subassembly D-40838) over the edge of the plate holder, and clamp the plate holder in position by turning part A-36928, subassembly D-40838. To move the plate holder to different positions, just unclamp the plate holder (turn part A-36928) and manually slide the plate holder to the new position. To take a spectra, pull the dark

slide and turn part A-35035 until the plate contacts the field flattener.
BEFORE SLIDING THE PLATE HOLDER TO A NEW POSITION, BE
SURE TO LIFT PLATE OFF OF THE FIELD FLATTENER BY TURNING
PART A-35035.

To change photographic plates, flip-up the four plate holder retainers (part A-40844) so the plate is free and lift the plate out. To load a plate, just place the plate in the plate holder flip-down the four retainers over the corners of the plate.

Be careful to keep the photographic plate and field flattener clean because dirt or dust particles could tilt the photographic plate and ruin the resolution.

1.11 45 cm RAYCES CAMERA (Ref. Drawings D-43752 and D-43755)

This camera consists of the 45 cm, (f/5 optics) module (D-43755) and the f/5 Direct Photography Module D-43752. The camera uses the same plateholders, D-40841, as the 14 cm Bowen camera.

The three sets of push-pull screws, items 1 and 2 of D-43755, are for tilting the optics with respect to the photographic plate. This adjustment has been set by Boller & Chivens. If some tilt develops in the focal plane, this adjustment can be used to realign the camera.

Parts A-43763 and B-43761 of subassembly D-43755 are protective covers to be installed when the optics are exposed.

1.12 STORAGE STAND (Ref. Drawing D-43845)

To install the spectrograph on the telescope, point the telescope to the zenith and lift the spectrograph. When the mounting flange is about 1 cm

from the telescope mounting flange, install the mounting screws and pull the spectrograph up to the mounting surface. After installation, remove the storage stand from the spectrograph.

To remove the spectrograph from the telescope, mount the stand on the spectrograph and reverse the installation procedure.

2.0 ALIGNMENT INSTRUCTIONS

2.1 COLLIMATOR ALIGNMENT (Ref. Drawing E-35093)

The collimator mirror is mounted rigidly in its cell and no adjustments between the mirror and the cell should be made.

The entire mirror cell may be moved along the focus axis and may be adjusted in tilt. The cell is supported to the focus carriage of the collimator assembly through three long cap screws (item 12) which work against three push screws (item 17). The cell is tilted by adjusting the push screws differentially against the pull screws.

The primary alignment of the collimator mirror is accomplished by using a point source of light focused on the slit in such a way that the axis of the light source is normal to the spectrograph mounting face. The light source should also illuminate the entire collimating mirror. With the camera removed from the spectrograph, the area of the grating which is illuminated by the collimator can be seen in a darkened room. The tilt of the collimating mirror should be adjusted to center the illuminated area on the grating. Rotation of the grating turret will assist in observing this alignment. Note that the image will be elongated in the direction of dispersion.

2.2 COMPARISON SOURCE ALIGNMENT (Ref. Drawing C-44900)

The adjustment is that required for the slit illumination mirror (A-39037). The initial adjustment of this mirror can be checked by placing a piece of white paper over the spectrograph slit and operating the comparison source to see if the slit is uniformly illuminated. A second check consists of placing a white surface in the grating assembly in place of the grating and observing the illuminated area to see if the collimator is

fully illuminated. This can also be done by putting a mirror in place of the grating and looking directly at the collimator mirror through the camera opening. In either case if the collimator is not uniformly illuminated, the slit illumination mirror should be adjusted by rotation of its holder after loosening three screws (item 11) or by shimming the mirror. Shimming is required if the illumination is not uniform in the direction of dispersion whereas rotation may be used if the illumination is not uniform perpendicular to the direction of dispersion.

2.3 EXPOSURE METER ALIGNMENT (Ref. Drawing D-38986)

This alignment consists solely of adjusting the flat photometer mirror (item A-38989) with the plunger (B-27765) all the way in. This mirror just intercepts the edge of the collimator beam. With the point source imaged at the center of the slit as in Section 2.1, and the photomultiplier tube assembly removed from the collimator housing, the photometer mirror can be viewed through the field lens opening or the light from the mirror can be imaged on a piece of white paper located at approximately the front face position of the photomultiplier tube. This image should be centered and will appear elliptical in shape.

2.4 BOWEN OPTICS ALIGNMENT

This portion of the instruction manual is to describe a recommended procedure for the initial alignment of the Bowen camera. After the initial alignments are completed, the focusing adjustments for slight focus shifts due to temperature changes or other causes can be made at the spectrograph collimator focus.

2.4.1 Bowen Optics Assembly (Ref. Drawing D-35089)

This assembly was aligned at Boller & Chivens. The initial test for this assembly is to take spectra on the spectrograph to check the resolution of the complete camera assembly.

Should the camera, for any reason, be out of alignment, the proper sequence of adjustments is as follows:

- a. Adjust the corrector plate to be parallel with mounting flange.
- b. Center the corrector plate with respect to the thick mirror. (Centration).
- c. Focus the camera.

These procedures are discussed below in detail.

To adjust the corrector plate parallel to the mounting face, indicate to the three points on the corrector plate surface adjacent to the adjusting screws. Adjust the corrector screws (item 2) as necessary, measuring to the three points described above. Be sure to indicate at the extreme edge of the corrector because of the curvature of the corrector plate surface near the edge.

Centration

Place camera optics module, less the plateholder module on an optical bench, in front of a collimator. Place a pinhole at the focus of the collimator. Adjust the camera position so that the image formed by the camera optics is within 1 or 2mm of the axis of the camera optics. Set up a microscope to examine the image.

The image should be circularly symmetrical. Significant deviations from symmetry indicate coma, caused by decentration of the corrector plate. It will be necessary to recenter the corrector.

Four set screws define the radial position of the corrector. Before tightening a screw to push the corrector, always loosen the opposite screw. Never force a screw as you might break the corrector.

Move the corrector in the direction of the flare of the coma. As you near centration, the adjustment becomes rather critical. When no more improvement can be made in the radial symmetry of the image, make sure that all four adjusting screws are in contact with the corrector, recheck the image and correct again if necessary. Remember, never force the screws, light contact is adequate.

The procedure to focus the camera is as follows:

- a. Attach the plateholder module to the Bowen optics module. Using the same set up as described above in the corrector plate centering, move the pin hole back and forth to find the best focus on the field flattener and then measure the distance from the pin hole to the focus of the collimator.
- b. Now, calculate the amount the camera is out of focus by using the following formula:

$$\text{Camera focus distance} = \text{pin hole distance} \times \frac{(\text{F. L. Camera})^2}{(\text{F. L. Collimator})^2}$$

(from collimated position)

- c. Then place the camera on a surface plate such that its corrector plate surface is in an upward direction and indicate with a depth micrometer to the three points on

the corrector plate adjacent to the adjusting screws. (Because of the extreme curvature of the corrector plate at its surface, all readings must be made at the extreme edge). Adjust the three sets of push-pull screws (items 1 and 5) in such a manner that the optical plane of the corrector remains parallel to its original plane.

The adjustment is in the same direction as the pin hole (ie., pin hole away from focus - move camera away from focus).

Another procedure to focus the camera on the plane of the field flattener is as follows:

- a. Use the spectrograph collimator and find the best focus in the camera by moving the collimator in specific focus steps. This will tell you how far one has to move the collimator from its collimated position.
- b. Now, calculate the amount the camera is out of focus by using the following formula:

$$\text{Camera distance} = \left(\frac{\text{Distance collimator is from}}{\text{its collimating position}} \right) \times \frac{(\text{F.L. camera})^2}{(\text{F.L. collimator})^2}$$

- c. This is the same as step "c" above.

APPENDIX I
STANDARD GRATINGS AVAILABLE

BOLLER & CHIVENS MODEL 31523 CASSEGRAIN SPECTROGRAPH

140 mm BOWEN-SCHMIDT CASSEGRAIN CAMERA *

STANDARD GRATINGS

Catalog Blaze	Grooves Per mm	Grating Angle	1st Order		2nd Order		3rd Order		1974 Base Price US \$
			Central λ	Disp. Å/mm	Central λ	Disp. Å/mm	Central λ	Disp. Å/mm	
5000Å	300	4° 18'	4550	224.0					825
5000	600	8° 38'	4550	114.0					825
5000	1200	17° 27'	4550	59.1					1485
5000	1800	26° 45'	4550	39.6					2060
5000	2160	32° 41'	4550	32.7					2725
7500	300	6° 28'	6825	226.0	3412	113.0			825
7500	600	13° 00'	6825	116.0	3412	58.0			825
7500	1200	26° 45'	6825	59.5	3412	29.8			1485
7600	270	5° 53'	6916	251.0	3458	126.0			285
7615	300	6° 33'	6929	226.0	3465	113.0			285
8125	830	19° 42'	7393	85.8	3696	42.9			1000
8465	400	9° 44'	7703	173.0	3852	86.5			825
8465	830.8	20° 34'	7703	85.9	3852	43.0			1000
8600	300	7° 25'	7826	227.0	3913	114.0			825
8700	80	2° 00'	7917	822.0	3958	411.0			825
1.0 μ	300	8° 38'	9100	228.0	4550	114.0	3033	76.0	825
1.0 μ	600	17° 27'	9100	118.0	4550	59.0	3033	39.3	825
1.0 μ	1200	36° 52'	9100	58.1	4550	29.1	3033	19.4	1485
1.1 μ	400	13° 00'	1.001	171.0	5005	85.6	3336	57.0	825
1.2 μ	400	13° 54'	1.092	175.0	5460	87.5	3640	58.3	825
1.2 μ	1200	46° 04'	1.092	55.3	5460	27.7	3640	18.4	1485
1.25 μ	150	5° 23'	1.137	449.0	5685	225.0	3790	150.0	825
1.25 μ	600	22° 02'	1.137	119.0	5685	59.4	3790	39.6	825
1.3 μ	400	15° 00'	1.183	177.0	5915	88.5	3943	59.0	825
1.6 μ	400	18° 40'	1.456	178.0	7280	88.8	4853	59.2	825

* For dispersion using the 45 cm Camera divide D by 3.21.

* λ_{min} is 19.5 nm ✓ D 1.393

APPENDIX II

**FORMULAS FOR ASTRONOMICAL GRATING
SPECTROGRAPHS**

FORMULAE FOR ASTRONOMICAL
GRATING SPECTROGRAPHS

C. C. WHEELER

March 16, 1973

THE PERKIN-ELMER CORPORATION
BOLLER & CHIVENS DIVISION

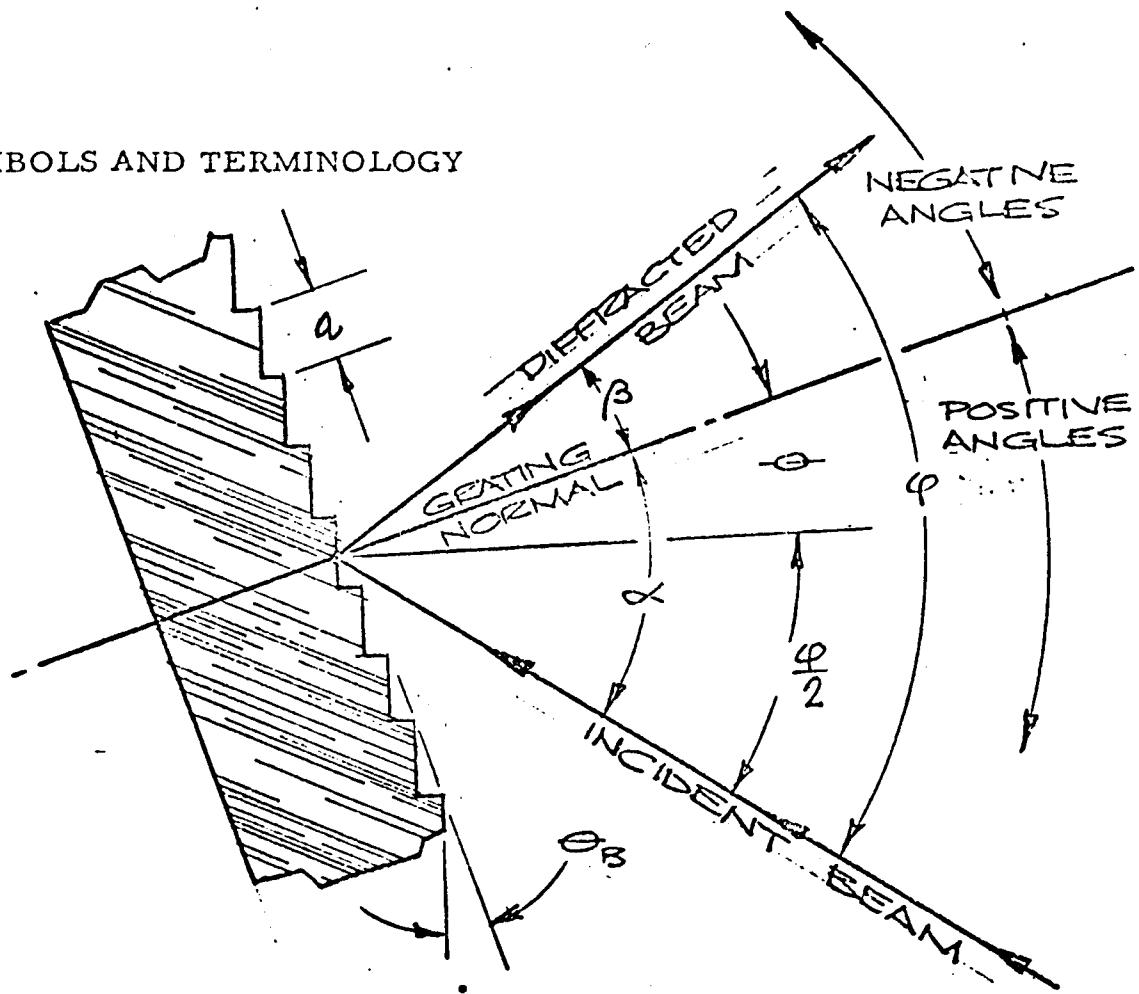
Revised May 20, 1975

INTRODUCTION

In this paper, the author brings together many formulae that are useful in the design and use of astronomical grating spectrographs. Many of these are standard formulae that are in general use. A few were derived by the author from standard formulae. No attempt has been made to reference the sources or to show the derivation of these formulae. This paper was intended primarily for the use of Perkin-Elmer personnel, however, it is available for general use.

Following the usual practice in astronomy, wavelengths are expressed in Angstroms.

1. SYMBOLS AND TERMINOLOGY



- λ = Wavelength in Angstroms (\AA)
- n = Grooves/mm
- a = Groove spacing in Angstroms = $10^7/n$
- m = Spectral order number
- α = Angle between incident ray and grating normal
- β = Angle between reflected ray and grating normal
- φ = Angle between incident and diffracted rays = $\alpha - \beta$
(Angle between Collimator and Camera)
- θ = Angle between grating normal and bisector of
incident and diffracted rays = $(\alpha + \beta)/2$
- λ_b = Blaze wavelength in \AA (First Order)
- λ_c = Wavelength at center of dispersed spectra in \AA
- θ_b = Blaze Angle
- D = Plate Dispersion $\text{\AA}/\text{mm}$
- F = Focal length of the spectrograph camera
- R = Free spectral range (separation, in Angstroms,
between adjacent orders)
- M = Grating magnification
- L = Length of one free spectral range

SIGN CONVENTION:

Angles on incident side of grating normal are positive.
Angles on opposite side of grating normal are negative.

2. GENERAL CASE

This section is applicable to all grating spectrographs, and particularly to the conventional Cassegrain and coude spectrographs. Echelle spectrographs, Littrow spectrographs and spectrographs using twice through correctors are special cases for which the general case applies, but can be treated in a simplified manner.

2.1 WAVELENGTH RELATIONSHIPS

$$\lambda = \frac{a}{m} (\sin \alpha + \sin \beta) \quad (1)$$

$$\lambda = \frac{2a}{m} (\sin \theta \cos \varphi/2) \quad (2)$$

which can be written:

$$\lambda = \frac{2 \times 10^7}{mn} (\sin \theta \cos \varphi/2) \quad (3)$$

A grating produces many spectra, one for each spectral order. These spectra are superimposed. The overlap relationships can be found in the wavelength relationships of equations. Figure 2 is a chart that shows 8 orders separated to indicate the overlap.

2.2 BLAZE RELATIONSHIPS

For peak performance, at any specific wavelength, the blaze angle should nearly equal the grating angle.

$$\theta_b \approx \theta$$

In grating catalogs, the published blaze wavelength is given for the first order in the Littrow mode, ($\varphi = 0$). In other cases, the working blaze wavelength is given by the expression:

$$\lambda'_b = \frac{\lambda_b}{m} \cos \varphi/2 \quad (4)$$

Plate Position

O Order +

1st Order

2nd Order

3rd Order

4th Order

5th Order

6th Order

7th Order

8th Order

1.5 μ
1.4 μ
1.3 μ
1.2 μ
1.1 μ
1 μ
9000
8000
7000
6000
5000
4000
3000

1.5 μ
1.4 μ
1.3 μ
1.2 μ
1.1 μ
1 μ
9000
8000
7000
6000
5000
4000
3000

1.1 μ
1 μ
9000
8000
7000
6000
5000
4000
3000

1 μ
8000
9000
7000
6000
5000
4000
3000

8000
9000
7000
6000
5000
4000
3000

7000
6000
5000
4000
3000

7000
6000
5000
4000
3000

6000
5000
4000
3000

5000
4000
3000

5000
4000
3000

2.3 DISPERSION

$$D = \frac{a \cos \beta}{mF} \quad (5)$$

which can be expressed

$$D = \frac{10^7 \cos \beta}{mnF} \quad (6)$$

or:

$$D = \frac{\lambda_c}{2F} (\cot \theta + \tan \varphi/2) \quad (7)$$

2.4 FREE SPECTRAL RANGE

The free spectral range is the wavelength separation between the adjacent spectra of different orders. The term is used primarily with echelle spectrographs.

$$R = \lambda_c / m \quad (8)$$

The length of a free spectral range is

$$L = R/D = \lambda_c / mD \quad (9)$$

2.5 SPECTRAL LINE CURVATURE

The monochromatic slit images of all spectrographs are curved. Due to the short slits used, this is not apparent in most stellar spectra, but it must be considered in spectrometers particularly with long slits such as spectroheliographs. The following formulas apply:

$$C = \frac{1}{R} = \frac{\sin \alpha + \sin \beta}{F \cos \beta} = \frac{m \lambda}{aF \cos \beta} \quad (10)$$

$$R = \frac{F}{2} (\cot \theta + \tan \varphi/2) \quad (11)$$

In terms of wavelength, the spectral line curvature is:

$$d\lambda/\lambda = h^2/2F^2 \quad (12)$$

h = slit height (1/2 slit length)

The slit image is concave as viewed from the longer wavelengths.

2.6 MAGNIFICATION CAUSED BY GRATING

Except for the Littrow, and zero order cases, a grating increases or reduces the width of the slit image. There is no change in the slit length. This is known as the anamorphic effect. This effect can be significant, particularly at high angular dispersions. The magnification is equal to:

$$M = \frac{\cos \alpha}{\cos \beta} = \frac{\cos (\theta + \varphi/2)}{\cos (\theta - \varphi/2)} \quad (13)$$

also

$$M = \frac{1 - \tan \theta \tan \varphi/2}{1 + \tan \theta \tan \varphi/2} \quad (14)$$

and

$$\tan \theta = \frac{1 - m}{(1 + m) \tan \varphi/2} \quad (15)$$

for example, if $\varphi = 50^\circ$, and

$$\theta = 30^\circ$$

$$M = \frac{\cos (30^\circ + 50^\circ/2)}{\cos (30^\circ - 50^\circ/2)} = 0.576$$

2.7 ASTIGMATISM

If the incident beam is not collimated, the grating will introduce astigmatism into the dispersed beam by shifting the tangential focus. There is no change in the sagittal focus. If we let S_s be the slit image distance of the incident beam, the distance to the sagittal image is

$$S_s = S_1$$

and to the tangential image

$$S_T = S_1 / M^2 = S_1 \left(\frac{\cos^2 \beta}{\cos^2 \alpha} \right) \quad (16)$$

If the incident beam is truly collimated, there is no astigmatic effect.

3.0 LITTRROW CASE

The Littrow configuration is seldom used in stellar spectrographs but very common in solar spectrographs. The collimator also serves as the camera optics. Consequently $\varphi = 0$ and $\alpha = \beta = \theta$. The following formulas apply to this special case:

3.1 WAVELENGTH

$$\lambda = \frac{2a}{m} \sin \theta \text{ (or } \alpha \text{ or } \beta \text{)} \quad (17)$$

3.2 DISPERSION

$$D = \frac{a \cos \theta}{mF} \quad (18)$$

which may be expressed

$$D = \frac{10^7 \cos \theta}{mnF} \quad (19)$$

or

$$D = \frac{\lambda_c}{2F \tan \theta} \quad (20)$$

3.3 SPECTRAL LINE CURVATURE

$$C = 1/R = \frac{2 \tan \theta}{F} \quad (21)$$

3.4 TWICE THROUGH CORRECTOR CASE

In the spectrographs that use a Schmidt corrector plate that is attached to the grating (twice through corrector), the grating normal must coincide with the camera axis within a very few degrees.

Then: $\alpha \approx \varphi \approx 2\theta$

$$\beta \approx 0$$

$$\cos \beta = 1$$

then the following dispersion formulas apply:

$$D = \frac{a}{mF} \quad (22)$$

or

$$D = \frac{\lambda_c}{F \sin \alpha} \quad (23)$$

4. ECHELLE SPECTROGRAPHS

Echelle spectrographs use coarse gratings, operating at very high spectral orders and at steep angles. Typical values are:

n ; 30 to 100 g/mm

m ; 25 to 100

θ ; 63° and higher

φ ; $\approx 12^\circ$

In most eschelle spectrographs, φ , θ and F are constants. We may rearrange equation 7 to read:

$$C_d = \frac{\lambda_c}{D} = \frac{2F}{\cot \theta + \cot \varphi} \quad (24)$$

We will call C_d the "dispersion constant", and

$$D = \lambda_c / C_d \quad (25)$$

The length of a free expected range can be stated as

$$L = C_d / m \quad (26)$$

APPENDIX III
DRAWING LISTS

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TASK #100

BRERA OBSERVATORY: ITALY

JOB NO. 59007

CASSEGRAIN SPECTROGRAPH

DATE 11-5-74

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二

TASK #100

L. 43488

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DATE 11-21

DATE 11-21

SHEET 2 OF 2

SHEET 2 OF 2

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DRAWING PAET NAME

B-37196 Cover Plate (Comp. Grating)

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Terminal End Plate

1

Wiring Diagram

109

Optical Diagram

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E-43839 Housing (Sheet 1 - Casting Dw

1000

E-43839 Housing (Sheet 2 - Machining Dwg.) Ref.

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DRAWING No.	PART NAME	No. Rev'd Per Next Assy.	Old Print	Tracing	Tracing Revised	Vendor Print	Shop Print	ISSUED FOR			Quart L fin.	
								No. Riv'd Tools Job	PURCH	MFR	MACH	
B-37196	Cover Plate (Comp. Grating)	1						1/8	7/4			
B-41064	Terminal End Plate	1						3/2	7/5			
C-41067	Wiring Diagram		Ref. Q					2/8	7/5			
D-43800	Optical Diagram		Ref. S					2/8	7/5			
E-43839	Housing (Sheet 1 - Casting Dwg.)	1						2/8	7/5			
E-43839	Housing (Sheet 2 - Machining Dwg.)	Ref.						1/29	7/5			

26703
Task #150

BRERA OBSERVATORY, ITALY
CASSAGRAIN SPECTROGRAPH
SUB ASSEMBLY
SHUTTER

JOS NO. 59007
DATE 11-5-74
SHEET 1 OF 1

CPN	PART NAME	No. New Print Revise	Old Print Revise	Tracing Revise	Vendor Print	Sh. P. Print	No. Job	Sp. Job	PURCH	MFR	MACH	FIN	IRON	ACSY
D-26703	Sub Assembly - Shutter	1		✓✓	✓✓	✓✓	118/74							
C-19031	Shutter Shaft Housing	1												
A-19045	Shutter	1												
A-19046	Shutter Shaft Housing Cover	1												
A-22064	Shutter Knob	1												
A-26779	Shutter Shaft	1												
A-29186	Switch Actuator	1												

ISSUED FOR

COPA
PRINT

BRERA OBSERVATORY, ITALY
CASSEGRAIN SPECTROGRAPH
BOWEN OPTICS CAMERA
SUSPENSION ASSEMBLY
GEAR DRIVE ASSEMBLY
SUSPENSION ASSEMBLY

JOB NO. 59007
DATE 12-19-74
SHEET 1 OF
NO. E-43488
NO. D-35089

DRAWING No.	PART NAME	No. Rec'd Per Asy.	Old Print	Training	Technical Revisions	Vendor Print	Show Print	No. Rec'd Per Job
								Ref.
D-35089	Sub Assembly - Bowen Optics Camera	1						12/9/74
B-28794	Corrector Cell	1						
B-28795	Corrector Retainer	1						
A-28797	Screw Extension	3						
A-28798	Corrector Cell Seal	1						
C-30887	Optical Diagram							
B-30889	Mirror Retainer	1						
C-35427	Bowen Optics	1						
D-35963	Housing	1						
D-42410	Flange	1						

ISSUED FOR

SHEET 1 OF 5
DATE 12-19-74
JOB NO. 59007

BRERA OBSERVATORY, ITALY
 GEOPHOTO ASSEMBLY
 SUB-ASSEMBLY
 HOLLOW CATHODE TUBE

JOB NO. 59007
 DATE 11-5-74
 SHEET 1 OF 1

NO. E-43488
 NO. C-35092

DR. NO. Ref.	PART NAME	ISSUED FOR										Qnt. Fin.	
		No. Drd Per Nxt Assy.	Old Print	Tracing	Tracing Revised	Vendor Print	Shno Print	Qty. Req'd This Job	PURCH	MFR	MACH	FIN	
JC-35092	Sub Assembly - Hollow Cathode Tube	1		✓✓	✓✓	1 1/8	1/4	1					
A-23315	Large Diffuser	1				Δ	2						
B-35825	Cam Modification	1				1 1/8	1/4	1					
C-35826	Extension Tube	1				↓	1						
S-43446	Diffuser Cell	1				↓	1						

BRERA OBSERVATORY

CASSEGRAIN SPECTROGRAPH

SUB ASSEMBLY

COLLIMATOR

NO. E-43488

NO. E-35093

DRAWING NO.

PART NAME

ISSUED FOR

Count

Part

Print

Assy

No. Rec'd

Per

Net Assy.

Job

Re'd

This

Job

Assy

Purch

Mfr

Mach

Fin

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Assy

Tracing

Revised

Vendor

Plant

Shop

Plant

Revised

Tracing

Old

Print

Assy

Assy

Retainer

Spacer

Spacer

Pad

Shaft

Spacer

Button

Guide

Assy

Retainer

Spacer

Spacer

Pad

Shaft

Spacer

Button

Guide

Assy

Retainer

Spacer

Spacer

Pad

Shaft

Spacer

Button

BRERA OBSERVATORY, ITALY
 CASSEGRAIN SPECTROGRAPH
 CATHODE TUBE POWER SUPPLY

NO. E-43488
 NO. C-35819

JOB NO. 59007
 DATE 11-5-74
 SHEET 1 OF 1

ENCL. NO.	PART NAME	Printed Part Number	Old Firm	Tracing	Tracing Revision	Vendor Print	Chap. No.	Chap. Fin.	No. Traced This Job	Quant. Fin.
C-35819	Sub Assembly	2)	1			✓✓	1/8/74			
C-35820	Chassis		1							
A-35821	Bracket		2							

ISSUED FOR

Quan.
Fin.

Purch

Mfr

Mach

Fin

M.P.

Assy

BRERA OBSERVATORY, ITALY

CASSEGRAIN SPECTROGRAPH

EXPOSURE METER

5900 NO. 800

DATE 11-6-7

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CUST. NO. 59007

SHEET 1 OF 1

BRERA OBSERVATORY, ITALY

CASSEGRAIN SPECTROGRAPH

SLIT

NO. E-43488

DATE 11-6-74

NO. D-39013

STREET 1 OF 1

DRAWING No.	Part No.	Description	QTY	QTY Issued	No. Issued Job	ISSUED FOR
D-39013	C-19409	Sub Assembly - Slit Mount	1	✓	1/8/74	Issued on Job 58957
C-19410	B-19414	Micrometer Mount Decker Guide	1 2	△	1/8/74	Issued on Job 58957
B-19416	B-19417	Decker Dial Index Decker Drive Arm	1 1	△	1/8/74	Issued on Job 58957
A-19418	A-19419	Decker Drive Shaft Decker Rack (Mod.)	1 1	△	1/8/74	Issued on Job 58957
A-19420	A-19422	Decker Pinion (Mod.) Spring Rod	1 2	△	1/8/74	Issued on Job 58957
A-19423	A-19609	Micrometer Clamp Special Set Screw	1 4	△	1/8/74	Issued on Job 58957
C-26755	B-26756	Decker Knob Decker	1 1	△	1/8/74	Issued on Job 58957
B-26758	A-26759	Decker Dial Shoulder Screw (Mod.)	1 1	△	1/8/74	Issued on Job 58957
B-35218	B-35219	Slit Jaw Slit Push Rod	1 Ea. 1	△	1/8/74	Issued on Job 58957
A-37194	A-37195	Spring Spring Guide	2 2	△	1/8/74	Issued on Job 58957
A-27828	A-27829	Field Lens Cell Field Lens	1 1	△	1/8/74	Issued on Job 58957
A-27833		Knurled Captive Screw	2			

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Task #240

1

JOB NO. 59007
DATE 12-19-74
SHEET 1 OF 1

NO D-40841

PLATEHOLDERS

1

Part No.	Part Name	Part No.	Part Name
V0-40841	Sub Assembly - Plateholders	1	Part No. 1 Part No. 2 Part Assy
C-35024	Dark Slide Retainer	1	
B-35025	Dark Slide	1	
A-35032	Dark Slide Handle	1	
A-35035	Thumbwheel	1	
A-35036	Diaphragm	1	
A-35037	Stud	1	
A-35038	Slug	3	
A-36291	Stop Ring	1	
A-36754-1	Dark Slide Stops	2	
A-36754-2	Dark Slide Stops	4	
A-36903	Thumbwheel Retainer	1	
C-40842	Placeholder Body	1	
C-40843	Placeholder Housing	1	
A-40844	Plate Clip	4	
A-40845	Spring Modification	4	

BRERA OBSERVATORY, ITALY
CASSEGRAIN SPECTROGRAPH
SLIT VIEWER

JOB NO. 59007
DATE 11-6-74
SHEET 1 OF 1

N.C. D-41010

Part No.	Part Name	No. Inv'd Per Ass'y.	Old Print	Tracing	Tracing Revised	Vendor Print	Shipped Print	No. Rec'd This Job
D-41010 C	Sub Assembly - Slit Viewer	1				✓✓	1/8/74	
C-41011 A	Eyepiece Mounting Tube	1						
B-41012	Entrance Cover Plate	1						
B-41013	Lock Collar	2						
B-41014 A	Retainer	1						
B-41015	Lens Tube	1						
B-41016	Mounting Sleeve	1						
B-41017 A	Rotation Collar	1						
A-41018	Mirror	1						
A-41019	Mirror Mount Cap	1						
A-41020-1A	Lens Cartridge	2						
A-41020-2A	Stop Cartridge	1						
A-41021	Mirror Mount	1						
A-41022	Mirror Mount Plug	1						
A-41023 A	Stop	2						
A-41024	Handle Modification	1						
A-41025	Retaining Ring	1						
S-43212	Eyepiece Stop	1						
A-43216	Eyepiece Modification	1					Y 11/18/74	
A-43638	Lock Screw	1					12/6/74 Z 1/26/74 Z	
A-43639	Lock lever	1	n					

TASK #130

43671

BRERA OBSERVATORY, ITALY
CASSEGRAIN SPECTROGRAPH
GRATING ASSEMBLY

JCS NO. 59007
DATE 12-18-74
SHEET 1 OF 1

NO. D-43671

ISSUED FOR

PRINTED PAPER

DRAWING NO.

PART NAME

No. Rev'd
N.A.Y.

Old Print

Tracing

Revised

Tracing

Revised

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Print

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F.in.

3/10/75

12/9/74



GRATING

Task #210

3755

BRERA OBSERVATORY

CASSEGRAIN SPECTROGRAPH

CASSEGRAIN SPECTROGRAPH

F/5 SPECTROGRAPHIC CAMERA

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SHEET 1 CE 1

DRIVER'S NAME	PART NAME	No. Reg'd	Old	New	Techno	Vendor	Ships	No. Cont.	ISSUED FOR
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Task #100

43845

BRERA OBSERVATORY

JOB NO. 59007

CASSAGRAIN SPECTROGRAPH

DATE 3-21-75

STORAGE STAND

SHEET 1 OF 1

NO. E-43488

NO. D-43845

DRAFTING

43845

CHISLOV

CASSAGRAIN

SPECTROGRAPH

PART NAME

No. 7014
P.L. Ass'y.

ISSUED FOR

DRAWING
NO.QUANT.
P.L.

ASSY

D-43845 Sub Assembly - Storage Stand

1

No. 7014
P.L. Ass'y.

ISSUED FOR

DRAWING
NO.QUANT.
P.L.

ASSY

D-35843 Stand

1

No. 7014
P.L. Ass'y.

ISSUED FOR

DRAWING
NO.QUANT.
P.L.

ASSY

A-43846 Guide Pin

2

No. 7014
P.L. Ass'y.

ISSUED FOR

DRAWING
NO.QUANT.
P.L.

ASSY

3/21/75

3/21/75

Task #250

DRAWING LIST

L- 44614

BRERA OBSERVATORY

CUSTODIAN

JOB NO. 59007

DATE 6-2-75

SHEET 1 OF 1

CASSEGRAIN ASSEMBLY

R.O. E-43488

JOB NO. 44614

FOCAL RATIO CONVERTER

DRAWING
NO.

PART NAME

No. Used
for
Part Assy.

Old Print

Tracing

Tracing
RevisedVendor
PrintShop
PrintNo.
Req'd
This
Job

Purch

MFR

MACH

FIN

IM3P

ASST

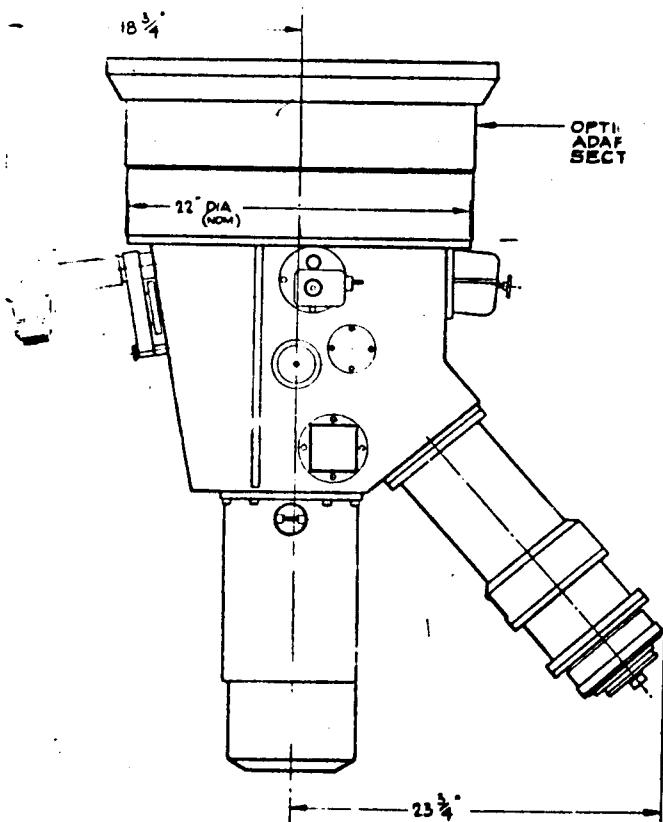
Mount.
Fin.

44614 Sub Assembly - Focal Ratio Conv. 1 SPN - 6/2/75

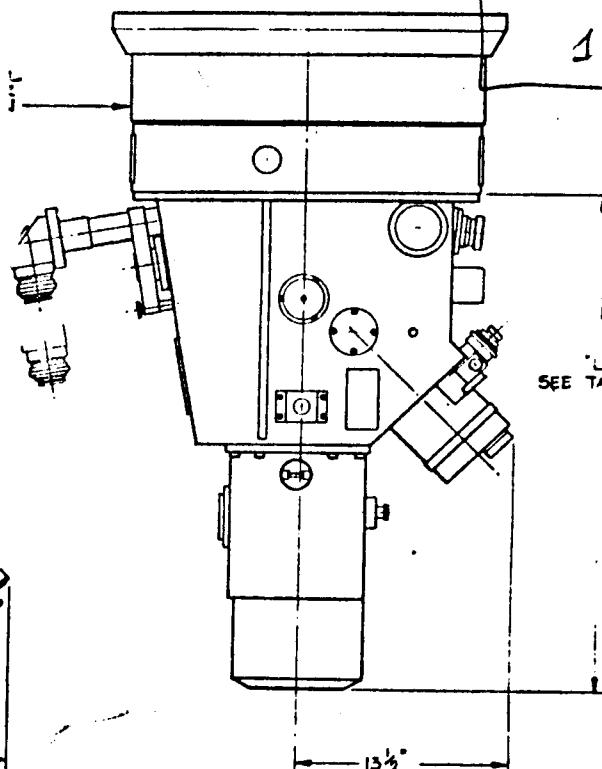
B-44613 Focal Ratio Converter Optics 1

ISSUED FOR

BOELLER & CHIVENS MODEL 31523 CASSEGRAIN SPECTROGRAPHS



TYPICAL SPECTROGRAPH
WITH IMAGE TUBE CAMERA
75 mm. COLLIMATOR



TYPICAL SPECTROGRAPH
WITH 100 mm. SCHMIDT CAMERA
AND 75 mm. COLLIMATOR

GENERAL DESCRIPTION

Boller & Chivens Model 31523 designates a family of highly efficient grating spectrographs designed for use at the Cassegrain focus of telescopes with apertures 30 inches in diameter or larger. Dispersions of .40 to .550 Å/mm can be used by the proper selection of cameras and gratings. Two types of cameras are available, flat field Schmidt for direct spectral photography and Schmidt Cassegrain cameras, with image tubes, for image intensified photography. Many optional features are available from existing designs and we can furnish custom designed components to serve specialized requirements.

The figures on this data sheet show the configuration and the optical arrangement of two typical examples of the Model 31523 Cassegrain spectrograph. The adapter section is designed to fit each specific telescope or it can be modified by an offset guider.

The standard collimator diameters are available, 75 mm., 90 mm., and 100 mm. The smaller collimator is adequate for Boller & Chivens' Schmidt photographic cameras, particularly when the spectrograph is used on smaller tele-

MECHANICAL SPECIFICATIONS

Telescope F/D	Length "L" (in) 75 mm. Collimator	Length "L" (in) 90 mm. Collimator	Length "L" (in) 100 mm. Collimator
8	31.5	35.8	38.9
10	37.5	42.9	46.8
12	43.5	50.0	54.7
14	49.5	57.1	62.6
16	55.5	64.1 → ←	70
18	61.5	71.2	7

scopes. With image tube cameras, the large collimator is preferred, especially with larger telescopes. The 90 mm. diameter is frequently selected in preference to the larger collimator, to limit the vignetting of the off-axis field. The focal ratio of the collimator will be selected to match the telescope on which it will be used. Although the length of the instrument usually depends on the focal ratio of the collimator, it may be shortened by using a special UV-transmitting conversion lens. The structure is unusually rigid to minimize deflections during long exposures.

Each spectrograph is thoroughly tested at our plant. With each spectrograph, we furnish three parfocalized plateholders, a stand for storage and maintenance, hardwood boxes for the cameras, plateholders and gratings, and a technical manual.

RAPPORTO INTERNO n° 7

CALCOLO TEORICO DELLA EFFICIENZA RELATIVA DEI
RETICOLI PER LO SPETTROGRAFO B&C DEL TELESCOPIO
RUTHS DA 137 CM DI MERATE.

R. FALOMO

MAGGIO 1982

OSSERVATORIO ASTRONOMICO DI BRERA

Via Brera, 28 - 20121 MILANO

Via E. Bianchi, 46 - 22055 MERATE (CO)

ITALY

Lo scopo di questo lavoro è di fissare un riferimento per i lavori spettroscopici che necessitino una calibrazione cromatica, per lo spettrografo B & C del telescopio Ruths.

I - INTRODUZIONE

Il telescopio Ruths dell'Osservatorio astronomico di Brera - Merate nella sua attuale configurazione viene impiegato per lavori di spettrografia utilizzando uno spettrografo della Boller and Chivens (vedi manuale d'uso della B & C) con un collimatore f/7 da ~ 63 cm e due camere Bowen-Schmidt una da 14 cm (FL) e l'altra da 45 cm.

La scala sul piano della fenditura è di circa 19.2 "/mm mentre sul piano focale delle camere, tenuto conto che l'ingrandimento è 0.22 con la camera corta e 0.71 con la camera lunga, è rispettivamente di 87.28 "/mm e 27.04 "/mm.

Attualmente sono disponibili 5 reticolari di diffrazione le cui caratteristiche sono riportate in tabella 3.

Nella tabella 2 sono invece riportate le lunghezze d'onda centrali dello spettro osservato (al I^o ordine) in funzione dell'angolo i di inclinazione del reticolo. Il range spettrale al primo ordine può essere dedotto infine dalla tabella 1.

TABELLA 1

RETICOLO tr/mm	400	600	1200
Camera 14 cm	6100	4000	2000
Camera 45 cm	1900	1200	650

Range spettrale

camera 19.5 mm

Mexico

TABELLA 3

Cat. N	(1) tratti/mm	(2) $a (\text{\AA})$	(3) θ_B	(4) λ_B	(5) M	(6) disp. 14 (\text{\AA}/mm)	(7) disp. 45 (\text{\AA}/mm)
35-53-17-590	400	25.000	13°54'	10920	0.79	175	54
35-53-17-580	400	25.000	9°44'	7703	0.85	173	54
35-53-17-260	600	16.667	8°38'	4550	0.87	114	35
35-53-17-350	600	16.667	13°00'	6825	0.81	116	36
35-53-17-530	1200	8.333	36°52'	9100	0.49	58	18

(1) numero tratti per mm

(2) $a = \text{inverso del n}^{\circ} \text{ di tratti per } \text{\AA}$ (3) $\theta_B = \text{angolo di blaze}$ (4) $\lambda_B = \text{lamda di blaze in configurazione non-littrow. } (\lambda_o = \text{lamda di blaze in catalogo})$

$$\lambda_B = \lambda_o \cos \frac{1}{2}(\alpha - \theta_B) = \lambda_o \cos \frac{\phi}{2} = 0.91 \lambda_o$$

$$\beta_B = i - \phi/2 ; \frac{n \lambda_B}{a} = \sin \alpha + \sin \beta_B$$

(5) ingrandimento causato dal reticolo

$$M = \frac{\cos \alpha}{\cos \beta} = \frac{1 - \tan \theta \tan \phi/2}{1 + \tan \theta \tan \phi/2}$$

(6) dispersione con la camera da 14 cm in $\text{\AA}/\text{mm}$ (7) dispersione con la camera da 45 cm in $\text{\AA}/\text{mm}$

GRATING WITH 400 GROOVES/MM CENTRAL WAVELENGTH

INCLINATION ANGLE	*	CENTRAL WAVELENGTH	*
5	*	3935.32	*
6	*	4755.77	*
7	*	5544.69	*
8	*	6331.96	*
9	*	7117.30	*
10	*	7900.47	*
11	*	8681.24	*
12	*	9459.36	*
13	*	10234.50	*

GRATING WITH 1200 GROOVES/MM

INCLINATION ANGLE	*	CENTRAL WAVELENGTH	*
13	*	3411.40	*
14	*	3669.76	*
15	*	3925.01	*
16	*	4180.06	*
17	*	4433.84	*
18	*	4686.36	*
19	*	4937.26	*
20	*	5186.76	*
21	*	5434.68	*
22	*	5680.94	*
23	*	5925.47	*
24	*	6168.19	*
25	*	6409.00	*
26	*	6647.94	*
27	*	6884.81	*
28	*	7119.58	*
29	*	7352.18	*
30	*	7582.55	*
31	*	7810.60	*
32	*	8036.28	*
33	*	8259.51	*
34	*	8480.22	*
35	*	8698.35	*
36	*	8913.83	*
37	*	9126.60	*
38	*	9336.58	*
39	*	9543.72	*
40	*	9747.96	*

GRATING WITH 600 GROOVES/MM

INCLINATION ANGLE	*	CENTRAL WAVELENGTH	*
8	*	4221.14	*
9	*	4744.68	*
10	*	5266.77	*
11	*	5787.26	*
12	*	6305.99	*
13	*	6822.79	*
14	*	7337.52	*
15	*	7850.02	*
16	*	8360.12	*
17	*	8867.67	*
18	*	9372.53	*
19	*	9874.53	*
20	*	10373.52	*

II - CALCOLO DELLA EFFICIENZA DEI RETICOLI

Usiamo le stesse notazioni del manuale B & C, come in fig.1. Quando il raggio diffratto è al centro dello spettro osservato, allora:

i = inclinazione del reticolo

$$\alpha = 24.5 + i$$

La distribuzione di luce $I(\beta)$ nello spettro prodotto da una luce bianca è
(D.Gray, The observations and analysis of stellar photospheres, 1976, pag.58):

$$I(\beta) = \frac{\sin^2 A}{A^2} \quad (1)$$

dove A vale:

$$A = n\pi \{ \cos \theta_B - [\sin \theta_B / \tan \frac{1}{2}(\alpha+\beta)] \} \quad (2)$$

La relazione tra l'angolo β e la lunghezza d'onda λ è:

$$\beta = \arcsen \left[\frac{\lambda n}{a} - \sin \alpha \right] \quad (3)$$

La λ_c al centro dello spettro osservato vale:

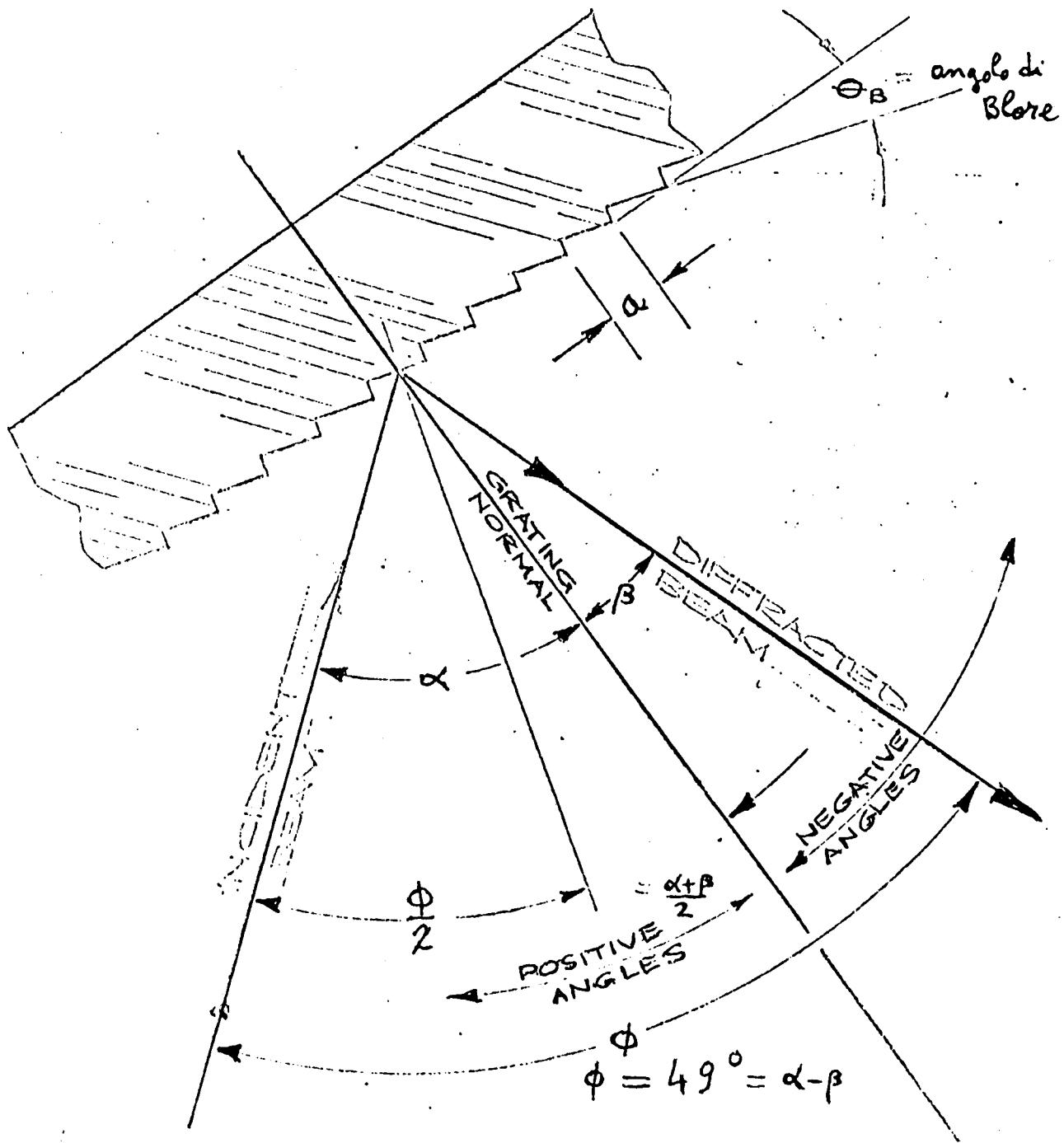
$$\lambda_c = \frac{a}{n} (\sin \alpha + \sin \beta_c)$$

$$\beta_c = -\frac{\phi}{2} + i = -24.5 + i$$

Utilizzando le relazioni (1), (2) e (3) e i dati di tab 1 è stata calcolata l'efficienza relativa dei 5 reticolni disponibili. Le curve delle fig 2, 3, 4, 5 e 6 riportano l'efficienza in funzione della lunghezza d'onda. Il tratto continuo si riferisce al primo ordine, quello tratteggiato al secondo ordine.

RINGRAZIAMENTI

Desidero ringraziare il Sig. G.Malaspina per la realizzazione al computer dei grafici di questo lavoro.



λ = lunghezza d'onda in \AA

n = n° d'ordine dello spettro

θ_B = angolo di Blaze

α = angolo tra raggio incidente e la normale al reticolo

β = " " " riflesso " " " "

ϕ = angolo tra il raggio incidente e diffratto = $\alpha - \beta$

(angolo tra collimatore e camera)

a = larghezza dei tratti in \AA

FIG 1

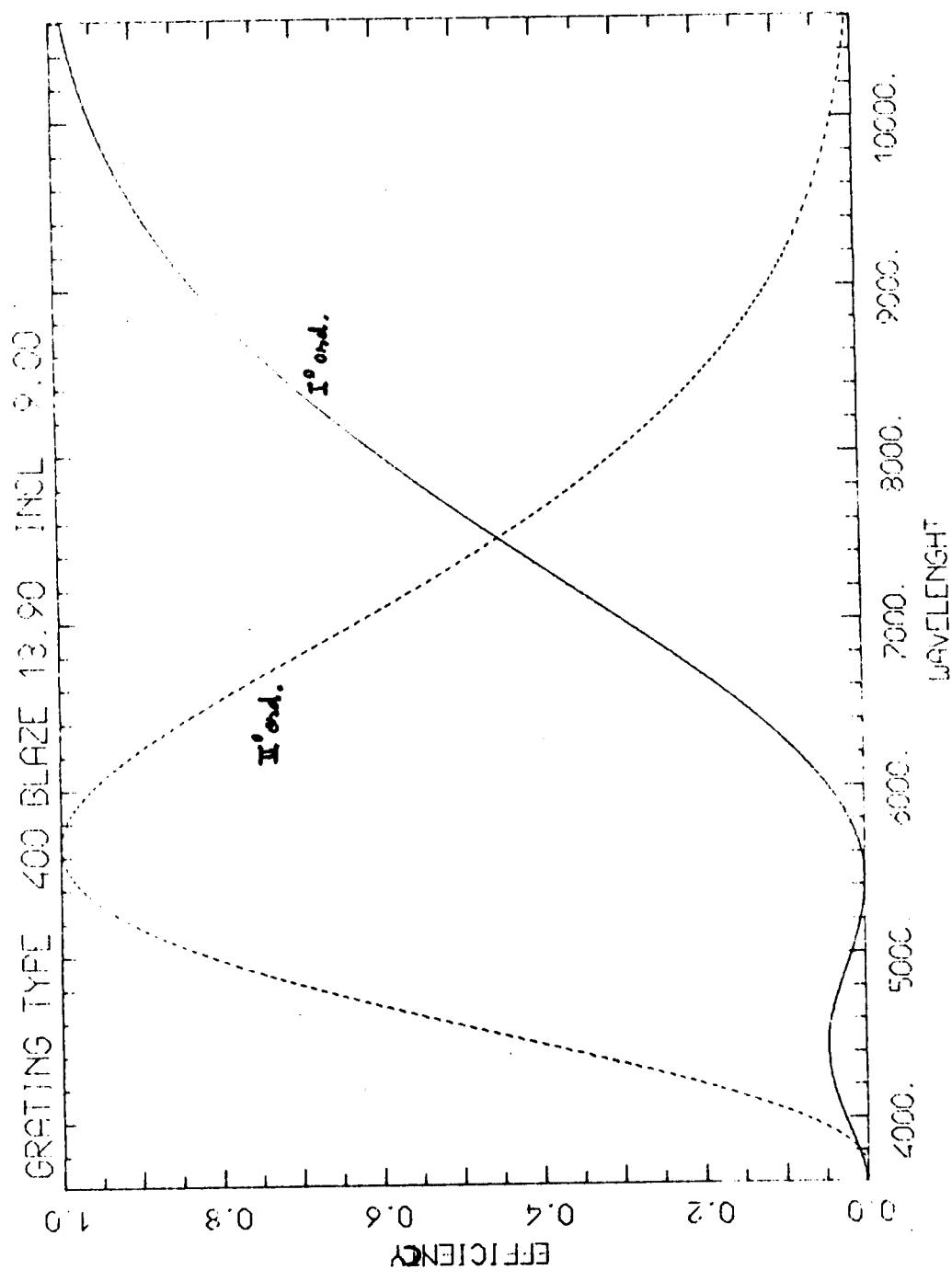


Fig 3

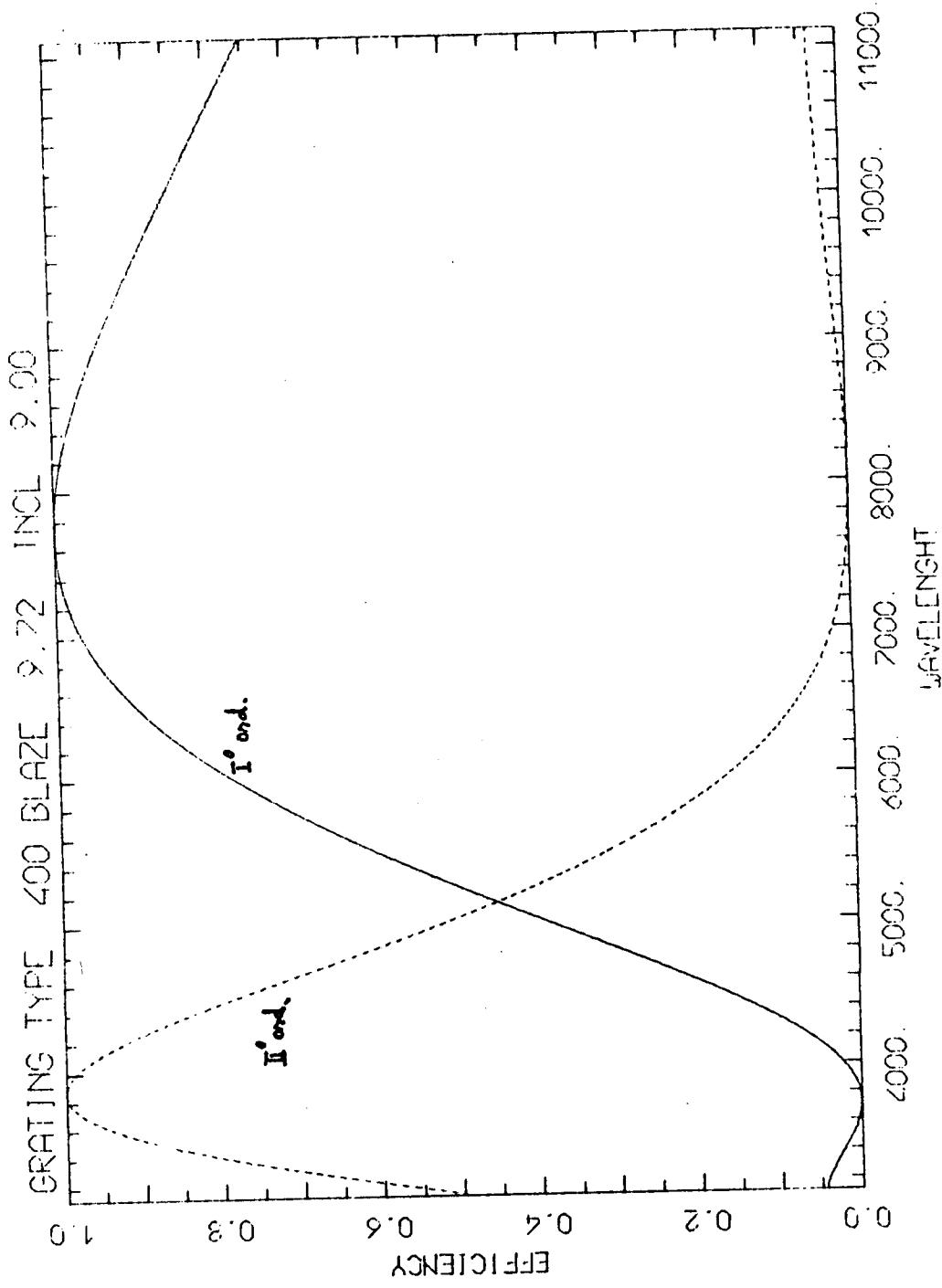


Fig 2

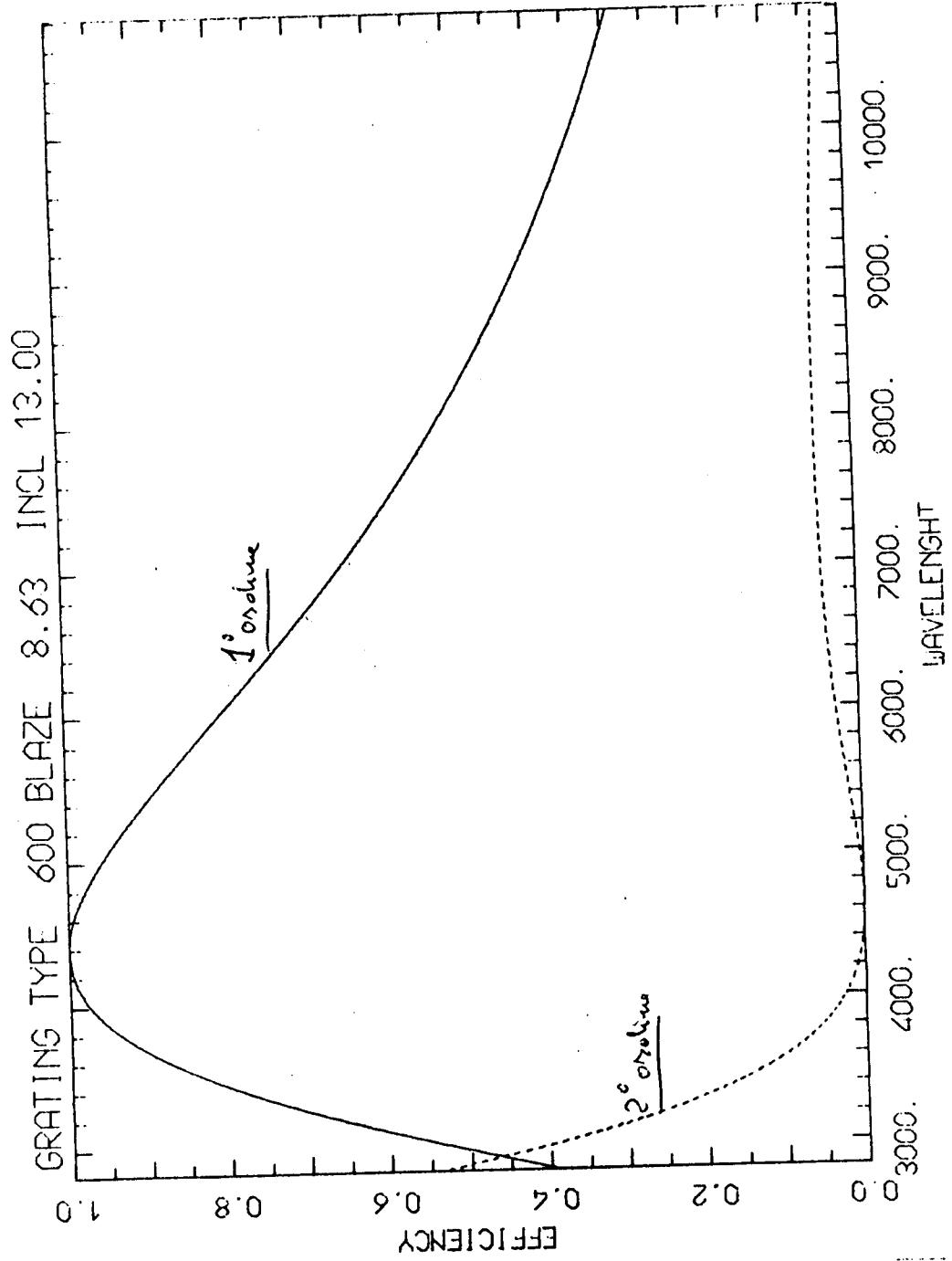


Fig 4

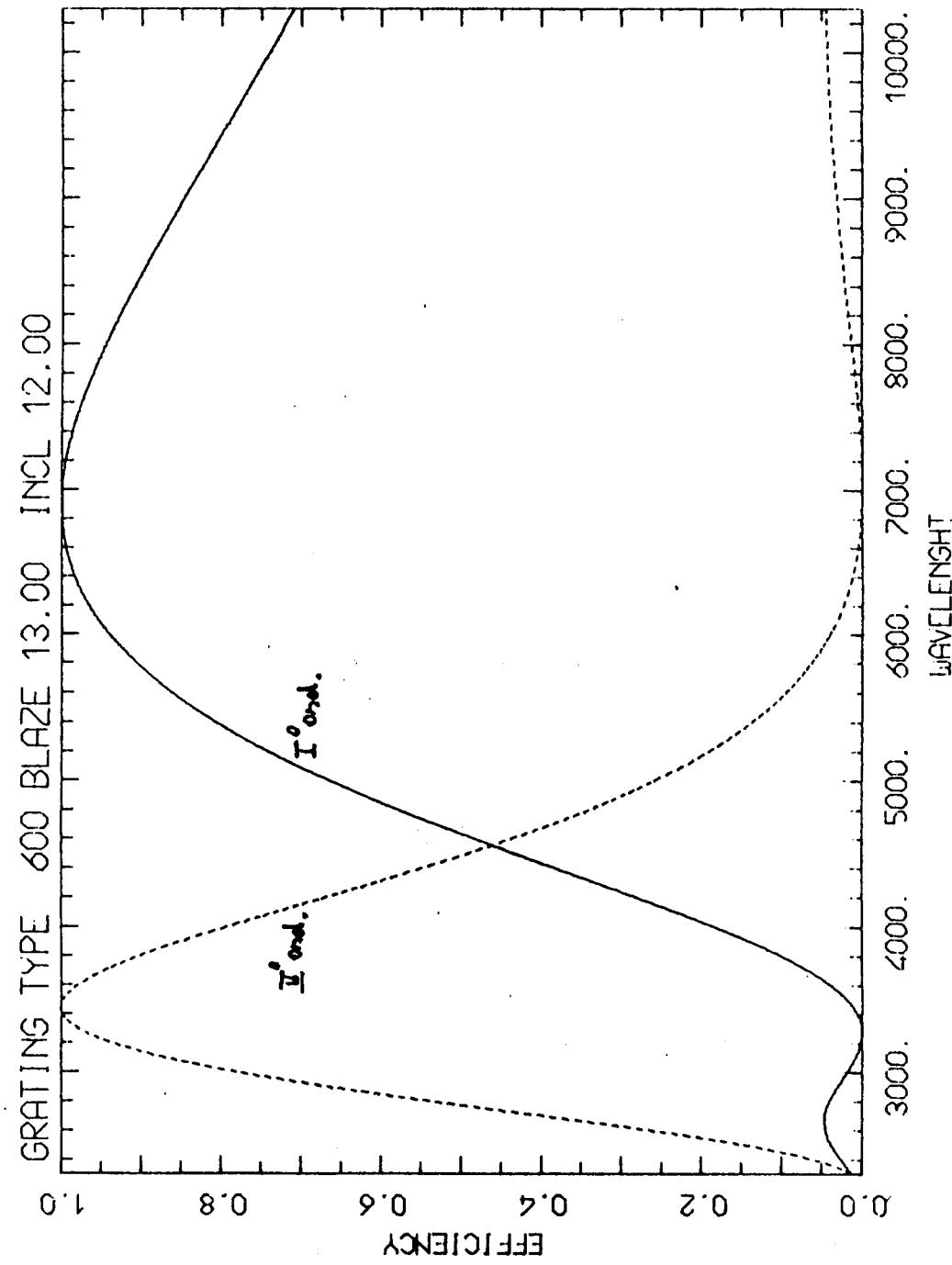


Fig 5

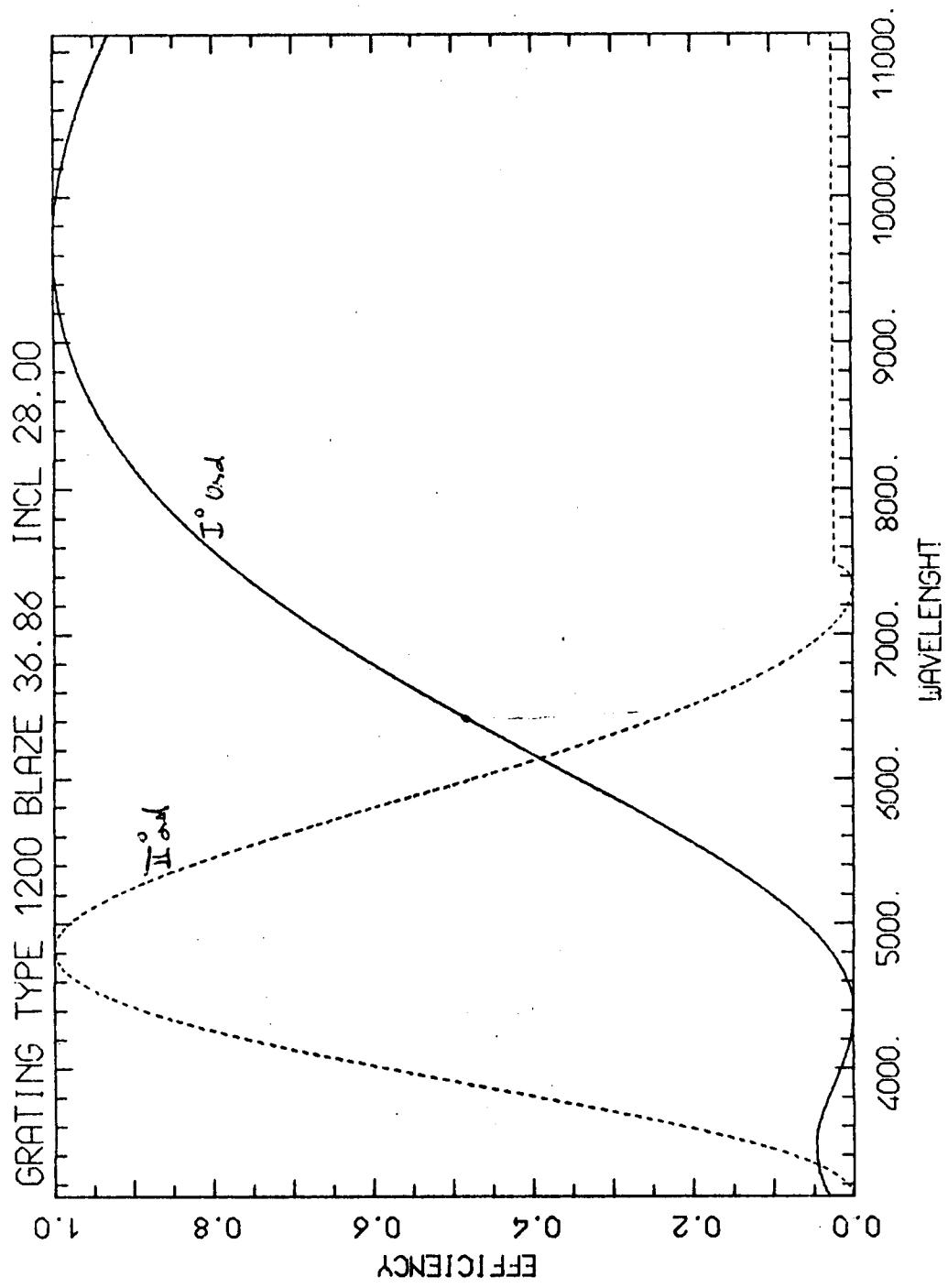


Fig 6

TABLE 1

The emission lines of the H-C Fe-A source of the B&C spectrograph

Wavelength (Å)	Identification	Notes
1 10830.337	A	Low Intensity Good
2 10470.054	A	Low Intensity Good
3 9784.503	A	Good
4 9657.786	A	Good
5 9354.220	A	Low Intensity Good
6 9224.499	A	Good
7 9122.975	A I	Good
8 8667.942	A I	Good
9 8521.442	A I	Good
10 8424.647	A I	(blend Good
11 8408.2	A I	(blend Good
12 8264.522	A I	Good
13 8115.311	A I	(blend Good
14 8103.692	A I	(blend Good
15 8014.786	A I	[blend Not good
16 8006.156	A I	[blend Not good
17 7948.175	A I	Good
18 7723.761	A I	Blend Good
19 7635.106	A I	Good
20 7514.650	A I	(blend Good
21 7503.868	A I	(blend Good
22 7383.981	A I	Good
23 7272.9	A I	Good
24 7147.042	A I	Low intensity Good
25 7067.2	A I	Good
26 6965.431	A I	Good
27 6871.3	A I	Low intensity Good
28 6752.8	A I	Low intensity Not good
29 6677.993	Fe I	Low intensity Not good
30 6416.3	A II	Low intensity Good
31 6172.4	A II	Blend Good
32 6114.9	A II	Low intensity Good
33 6043.2	A I	(blend Good
34 6032.1	A I	(blend Good
35 5912.1	A I	Low intensity Good
36 5888.6	A I	Low intensity Good
37 5495.9	A I	Blend Not good
38 5455.613	Fe I	(blend Not good
39 5446.920	Fe I	(blend Not good
40 5429.699	Fe I	Not good
41 5405.778	Fe I	(blend Not good
42 5397.131	Fe I	(blend Not good
43 5371.493	Fe I	Good
44 5328.534	Fe I	Not Good
45 5270.360	Fe I	Not Good
46 5227.192	Fe I	Not Good
47 5167.491	Fe I	Not Good
48 5141.8	A II	Low intensity Not good
49 5062.070	A II	Low intensity Not good
50 5017.160	A II	Blend Not good
51 4965.120	A II	(blend Good

52	4957.603	Fe I	: blend	Good
53	4879.9	A II	Blend	Good
54	4847.900	A II	Low intensity	Good
55	4806.070	A II	Low intensity	Good
56	4764.890	A II		Good
57	4735.930	A II	{ blend	Not good
58	4726.910	A II	{ blend	Not good
59	4657.940	A II		Good
60	4609.600	A II		Good
61	4589.930	A II		Good
62	4579.244	A II	{ blend	Good
63	4545.080	A II	{ blend	Good
64	4510.733	A I		Good
65	4481.630	A II	Low intensity	Not good
66	4404.8	Fe I	Low intensity	Not good
67	4383.547	Fe I	-	Good
68	4325.8	Fe I	Blend	Good
69	4200.	A I - Fe I	Blend	Good
70	4158.591	A I		Good
71	4103.910	A II		Good
72	4045.815	Fe I	Low intensity	Good
73	3886.284	Fe I		Good
74	3859.	Fe I	Blend	Good
75	3705.567	Fe I	Blend	Not good
76	3679.915	Fe I	Blend	Good
77	3647.844	Fe I	Low intensity	Good
78	3631.464	Fe I		Good
79	3618.769	Fe I		Good
80	3608.861	Fe I		Not good
81	3581.195	Fe I	Blend	Not good
				Good

Fig. 1

Fe An

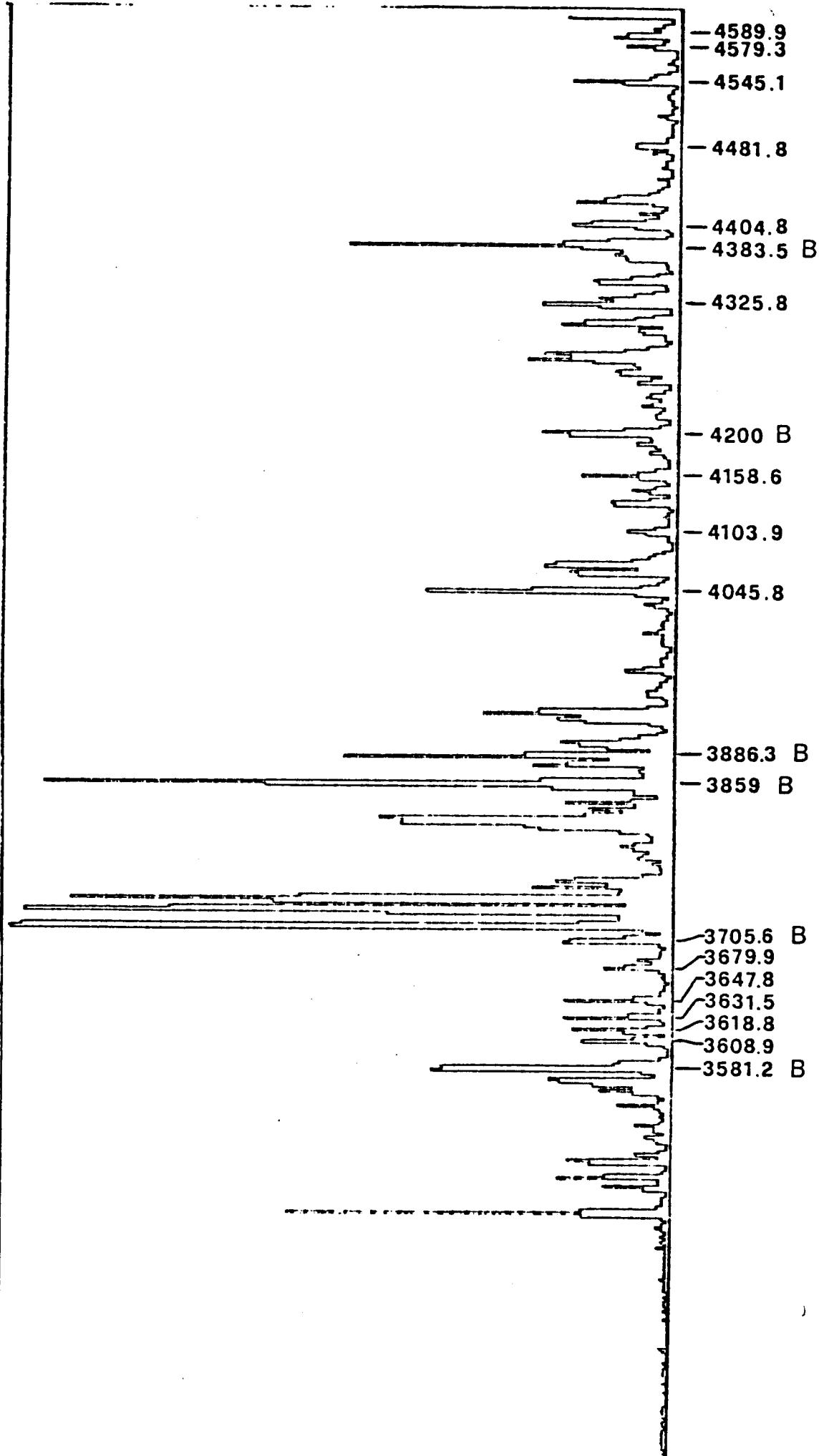


FIG. 2

Fe Ar

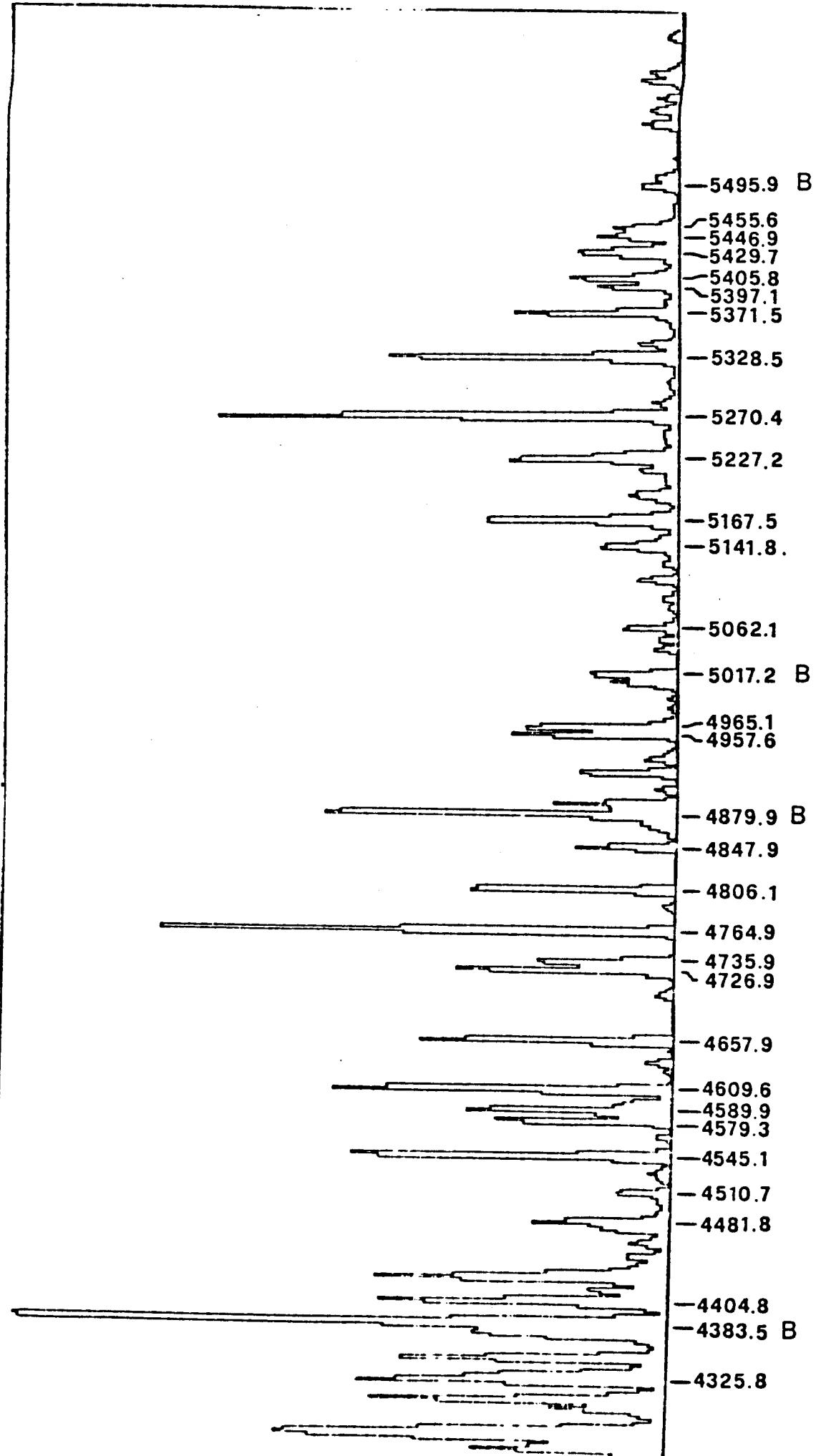


FIG. 3

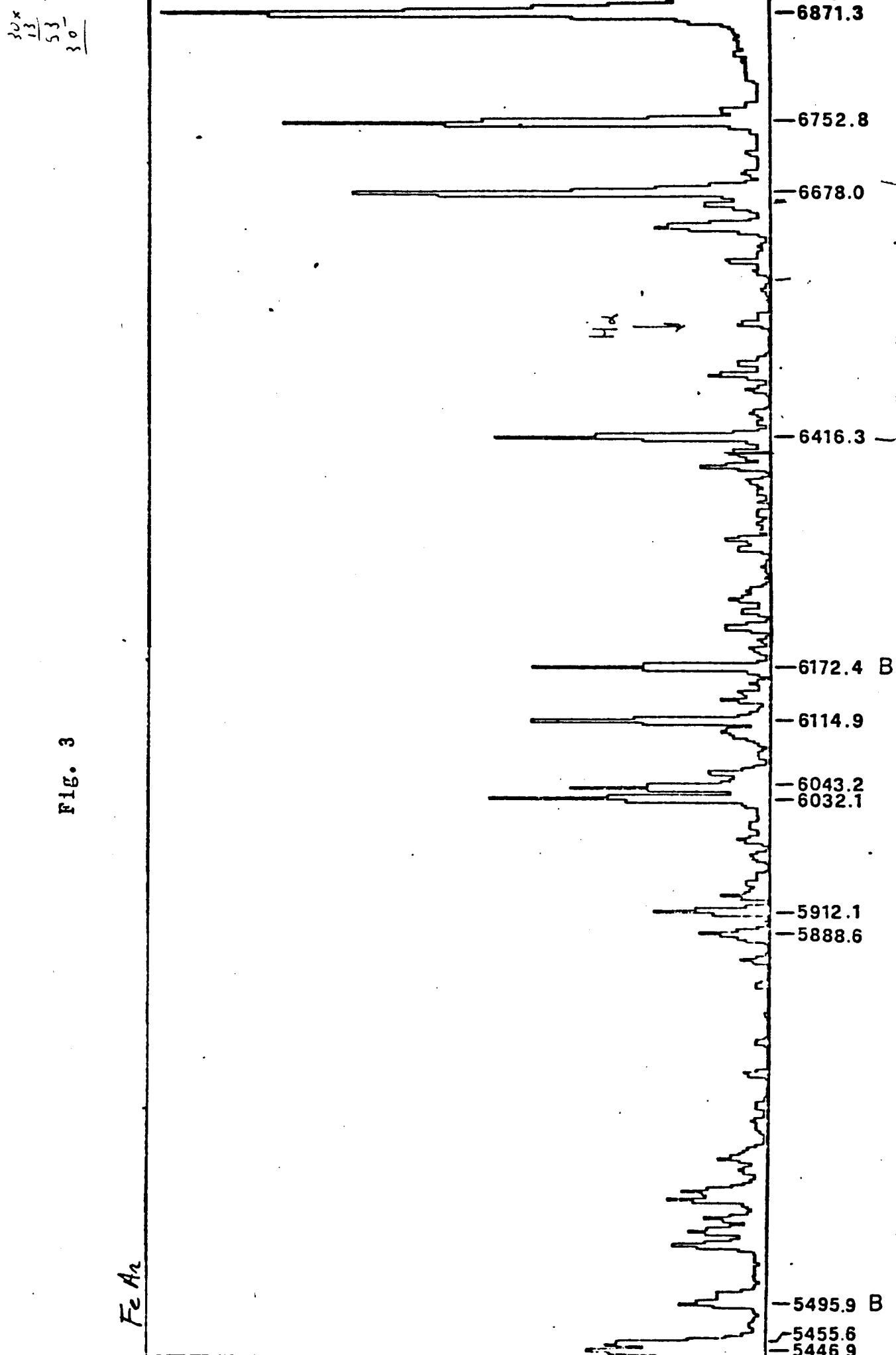


Fig. 4

Fe An

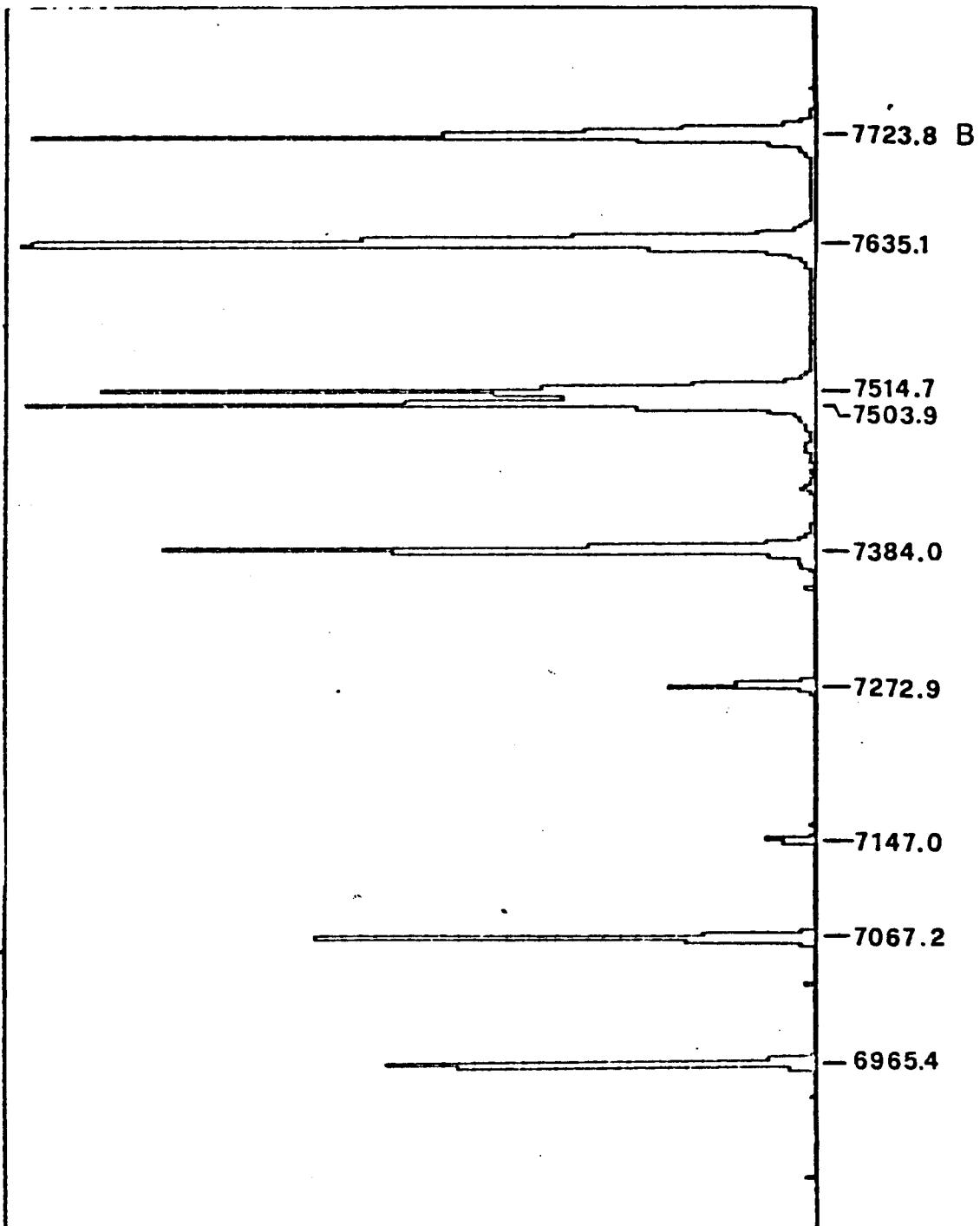
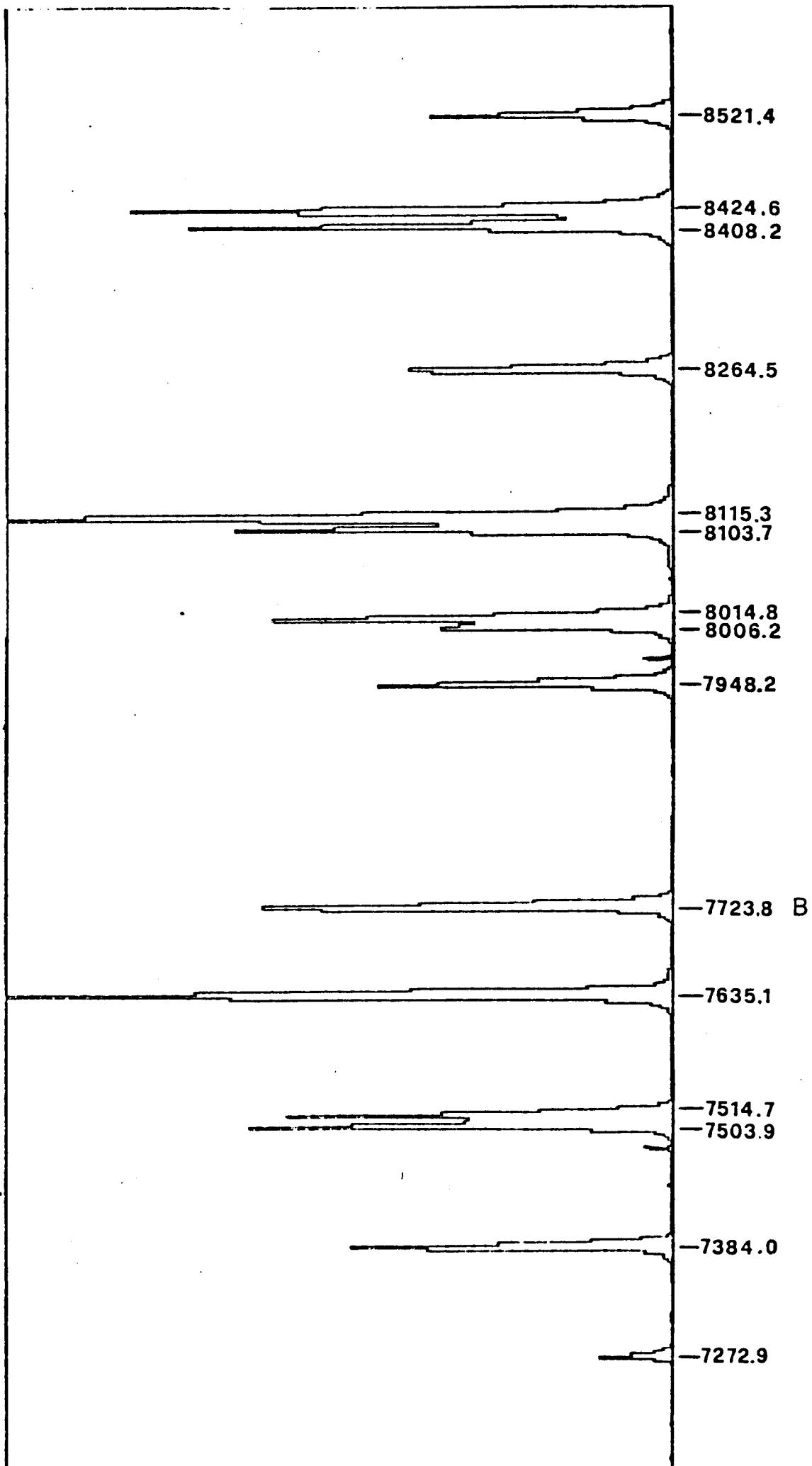


Fig. 5

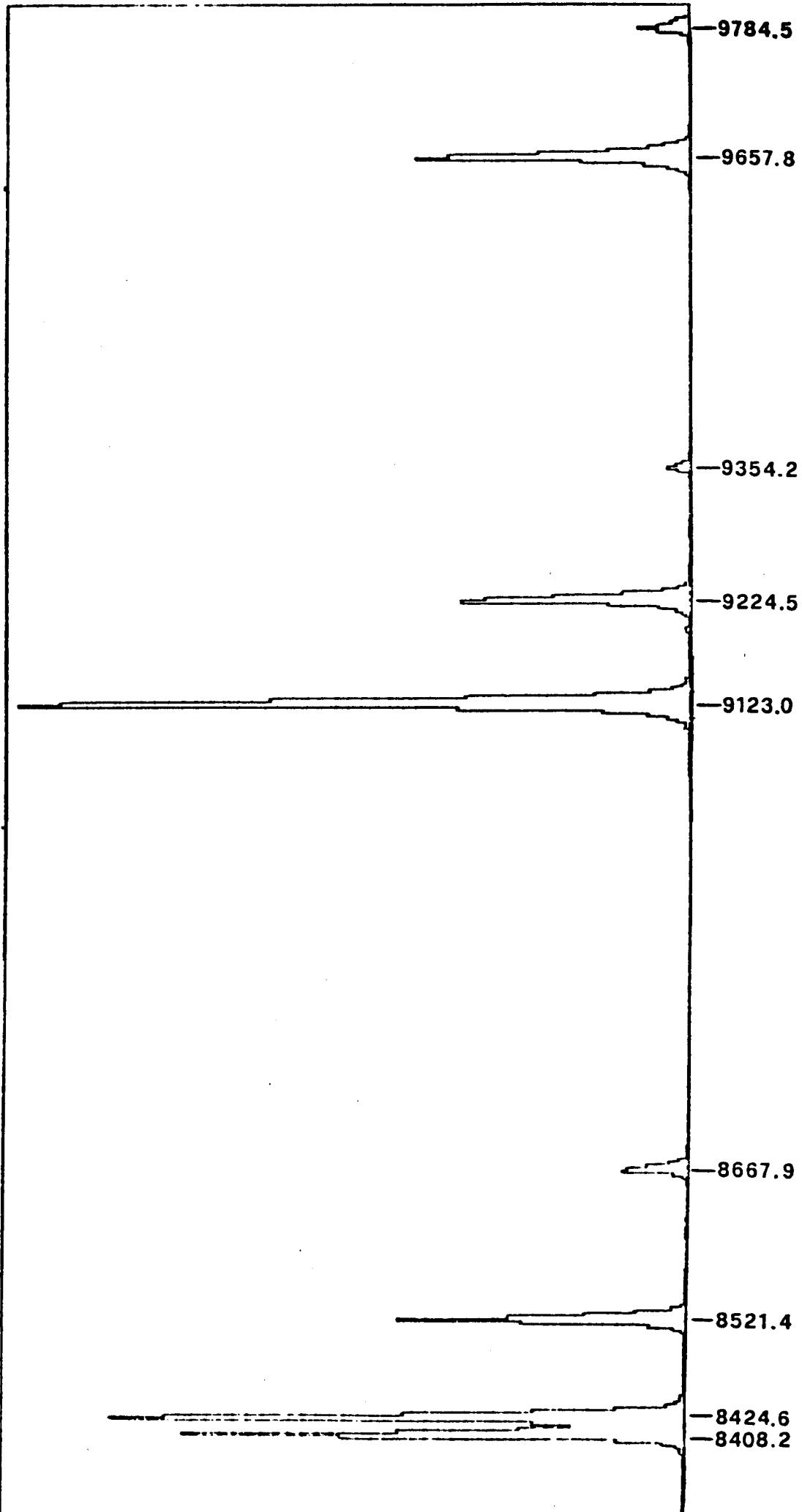
200
150
100
50

Fe A_e



Fe Ar

Fig. 6



RETIKOLO

RETIKOLO 400 TR/MM

Angolo	Lamda	Angolo	Lamda	Angolo	Lamda	Angolo	Lamda
4.9	3886.3	5.0	3965.4	5.1	4044.5	5.2	4123.6
5.3	4202.7	5.4	4281.7	5.5	4360.8	5.6	4439.8
5.7	4518.9	5.8	4597.9	5.9	4676.9	6.0	4755.8
6.1	4834.8	6.2	4913.8	6.3	4992.7	6.4	5071.6
6.5	5150.5	6.6	5229.4	6.7	5308.3	6.8	5387.1
6.9	5466.0	7.0	5544.8	7.1	5623.6	7.2	5702.4
7.3	5781.2	7.4	5859.9	7.5	5938.7	7.6	6017.4
7.7	6096.1	7.8	6174.8	7.9	6253.5	8.0	6332.1
8.1	6410.7	8.2	6489.3	8.3	6567.9	8.4	6646.5
8.5	6725.0	8.6	6803.6	8.7	6882.1	8.8	6960.6
8.9	7039.0	9.0	7117.5	9.1	7195.9	9.2	7274.3
9.3	7352.7	9.4	7431.0	9.5	7509.3	9.6	7587.7
9.7	7665.9	9.8	7744.2	9.9	7822.4	10.0	7900.7
10.1	7978.8	10.2	8057.0	10.3	8135.1	10.4	8213.3
10.5	8291.4	10.6	8369.4	10.7	8447.5	10.8	8525.5
10.9	8603.5	11.0	8681.4	11.1	8759.4	11.2	8837.3
11.3	8915.2	11.4	8993.0	11.5	9070.9	11.6	9148.7
11.7	9226.4	11.8	9304.2	11.9	9381.9	12.0	9459.6
12.1	9537.2	12.2	9614.9	12.3	9692.5	12.4	9770.0
12.5	9847.6	12.6	9925.1	12.7	10002.6	12.8	10080.0
12.9	10157.4	13.0	10234.3	13.1	10312.2	13.2	10395.5
13.3	10466.8	13.4	10544.1	13.5	10621.3	13.6	10698.5
13.7	10775.7	13.8	10852.8	13.9	10929.9	14.0	11007.0
14.1	11084.0	14.2	11161.0	14.3	11238.0	14.4	11314.9
14.5	11391.8	14.6	11468.7	14.7	11545.5	14.8	11622.3
14.9	11699.0	15.0	11775.8	15.1	3965.4	15.0	3965.4

LE LUNGHEZZE D'ONDA DEL 2° ORDINE

SI OTTENGONO DA QUELLE DEL PRIMO
ORDINE DIVIDENDO PER 2.

ESEMPIO :

Reticollo 400 tr/mm

$$i = 12.7 \quad \lambda(2^{\text{ord}}) = 10.002$$

$$\lambda(2^{\text{ord}}) = \frac{10.002}{2} = 5.001$$

RETICOLO 600 TR/MM

Angolo	Lamda	Angolo	Lamda	Angolo	Lamda	Angolo	Lamda
4.9	2590.9	5.0	2643.6	5.1	2696.3	5.2	2749.1
5.3	2801.8	5.4	2854.5	5.5	2907.2	5.6	2959.9
5.7	3012.6	5.8	3065.2	5.9	3117.9	6.0	3170.6
6.1	3223.2	6.2	3275.8	6.3	3328.5	6.4	3381.1
6.5	3433.7	6.6	3486.3	6.7	3538.9	6.8	3591.4
6.9	3644.0	7.0	3696.5	7.1	3749.1	7.2	3801.6
7.3	3854.1	7.4	3906.6	7.5	3959.1	7.6	4011.6
7.7	4064.1	7.8	4116.5	7.9	4169.0	8.0	4221.4
8.1	4273.8	8.2	4326.2	8.3	4378.6	8.4	4431.0
8.5	4483.4	8.6	4535.7	8.7	4588.0	8.8	4640.4
8.9	4692.7	9.0	4745.0	9.1	4797.3	9.2	4849.5
9.3	4901.8	9.4	4954.0	9.5	5006.2	9.6	5058.4
9.7	5110.6	9.8	5162.8	9.9	5215.0	10.0	5267.1
10.1	5319.2	10.2	5371.3	10.3	5423.4	10.4	5475.5
10.5	5527.6	10.6	5579.6	10.7	5631.6	10.8	5683.7
10.9	5735.6	11.0	5787.6	11.1	5839.6	11.2	5891.5
11.3	5943.4	11.4	5995.3	11.5	6047.2	11.6	6099.1
11.7	6150.9	11.8	6202.8	11.9	6254.6	12.0	6306.4
12.1	6358.2	12.2	6409.9	12.3	6461.6	12.4	6513.4
12.5	6565.1	12.6	6616.7	12.7	6668.4	12.8	6720.0
12.9	6771.6	13.0	6823.2	13.1	6874.3	13.2	6926.3
13.3	6977.9	13.4	7029.4	13.5	7080.9	13.6	7132.3
13.7	7183.8	13.8	7235.2	13.9	7286.6	14.0	7338.0
14.1	7389.3	14.2	7440.7	14.3	7492.0	14.4	7543.3
14.5	7594.5	14.6	7645.8	14.7	7697.0	14.8	7748.2
14.9	7799.4	15.0	7850.5	15.1	7901.6	15.2	7952.7
15.3	8003.8	15.4	8054.9	15.5	8105.9	15.6	8156.9
15.7	8207.9	15.8	8258.8	15.9	8309.7	16.0	8360.6
16.1	8411.5	16.2	8462.4	16.3	8513.2	16.4	8564.0
16.5	8614.8	16.6	8665.5	16.7	8716.2	16.8	8766.9
16.9	8817.6	17.0	8868.2	17.1	8918.8	17.2	8969.4
17.3	9020.0	17.4	9070.5	17.5	9121.0	17.6	9171.5
17.7	9221.9	17.8	9272.4	17.9	9322.7	18.0	9373.1
18.1	9423.4	18.2	9473.8	18.3	9524.0	18.4	9574.3
18.5	9624.5	18.6	9674.7	18.7	9724.8	18.8	9775.0
18.9	9825.1	19.0	9875.1	19.1	9925.2	19.2	9975.2
19.3	10025.2	19.4	10075.1	19.5	10125.0	19.6	10174.9
19.7	10224.8	19.8	10274.6	19.9	10324.4	20.0	10374.2

Romo { RG 630 minva 1 mm

~~RG 630~~

Giallo 66451 1 m

BG 23 - 14 1 m

063 (06590) (Gelb 10 mm) } 1 mm.
RG 610 (RG 1) }

(blu)

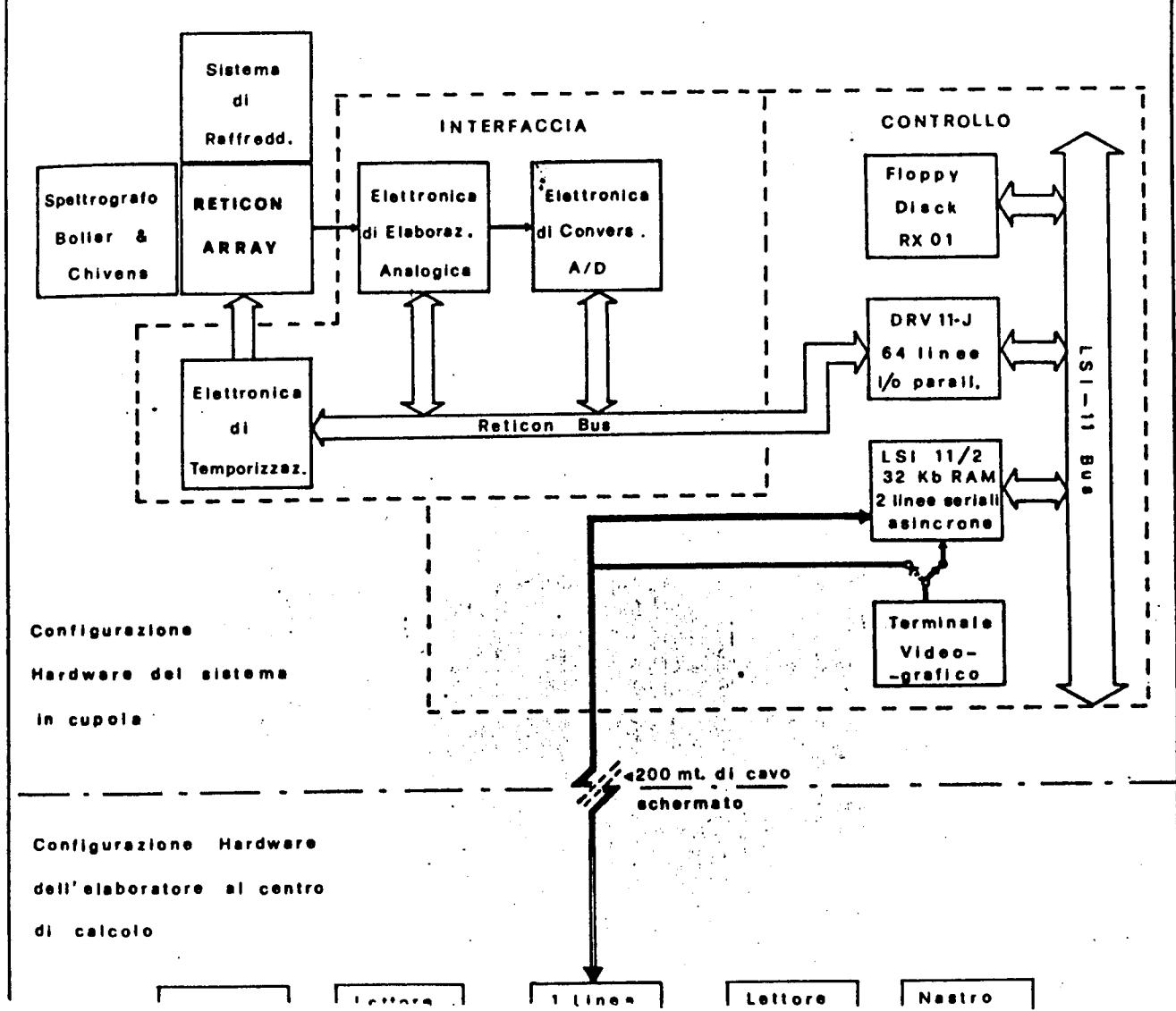
1 mm.

BG 33
~~10~~

(grigio)

GG 435
455

Schema a blocchi del sistema completo



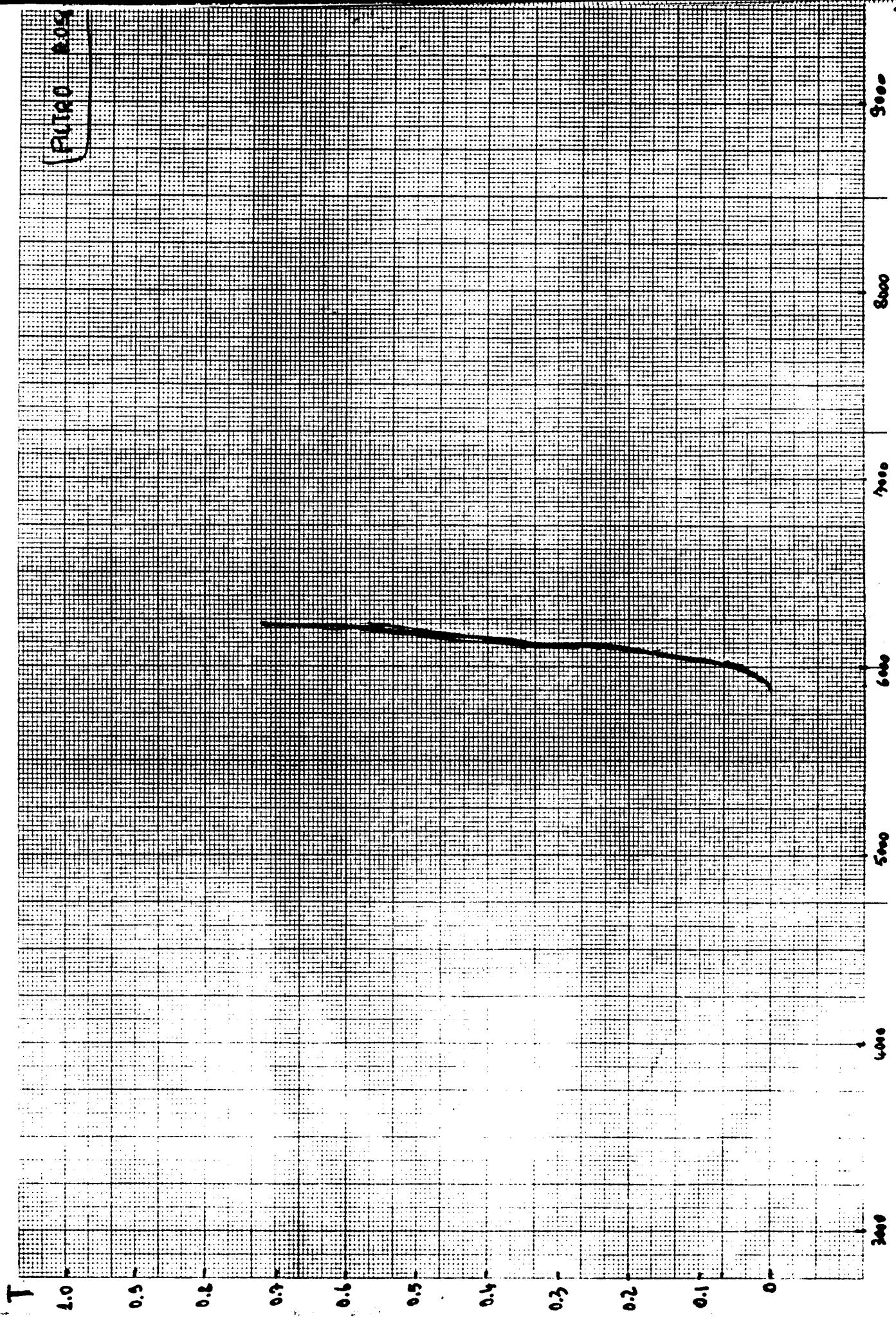
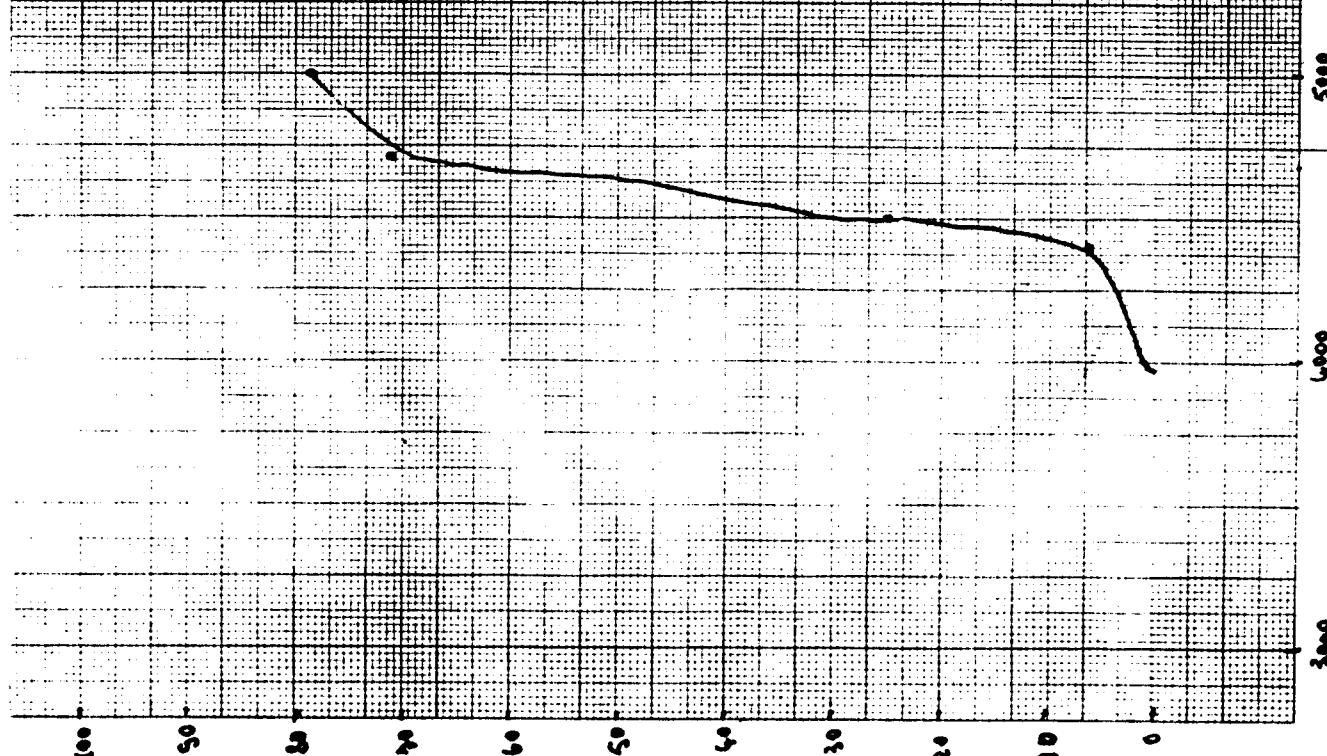
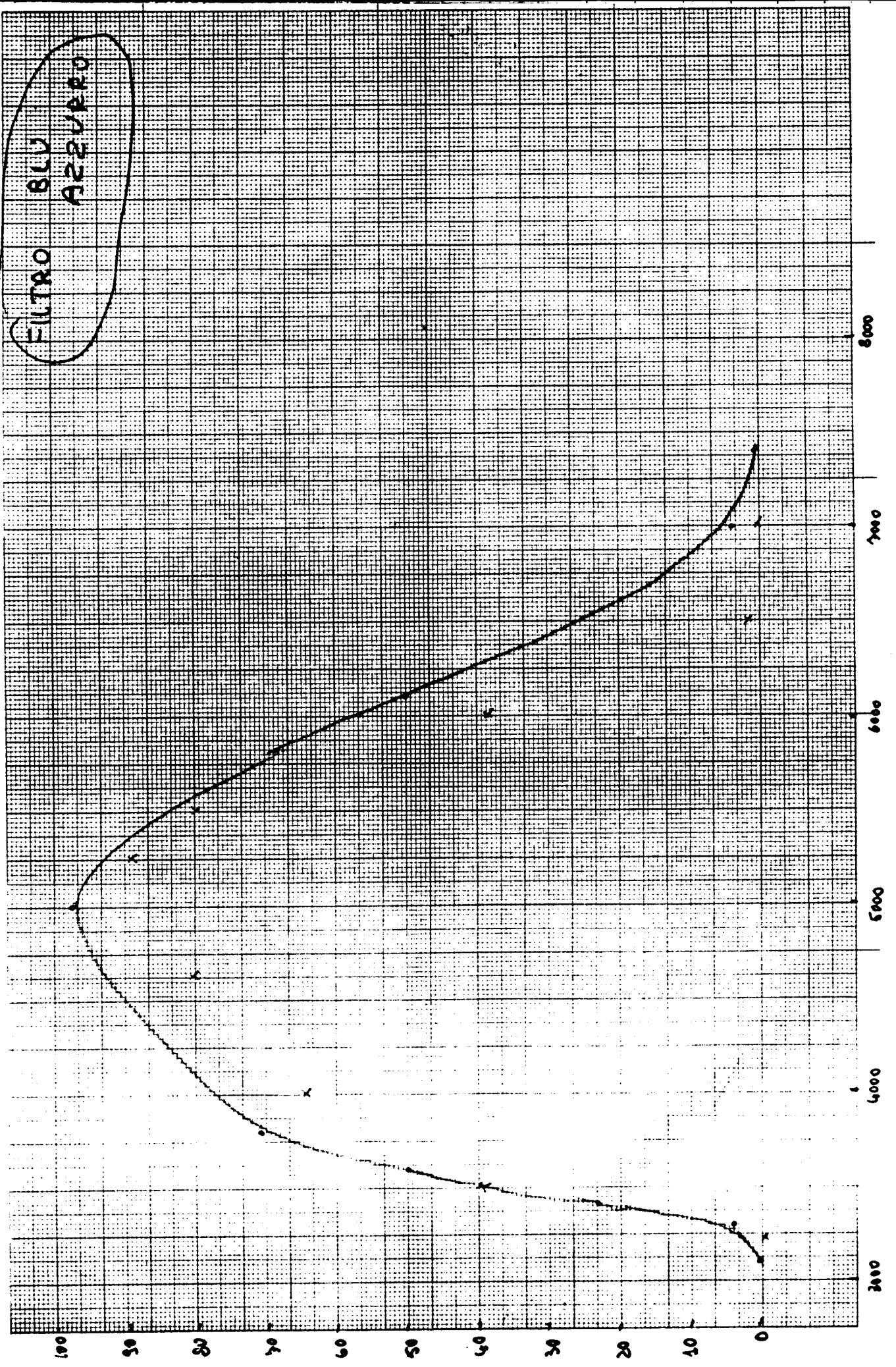
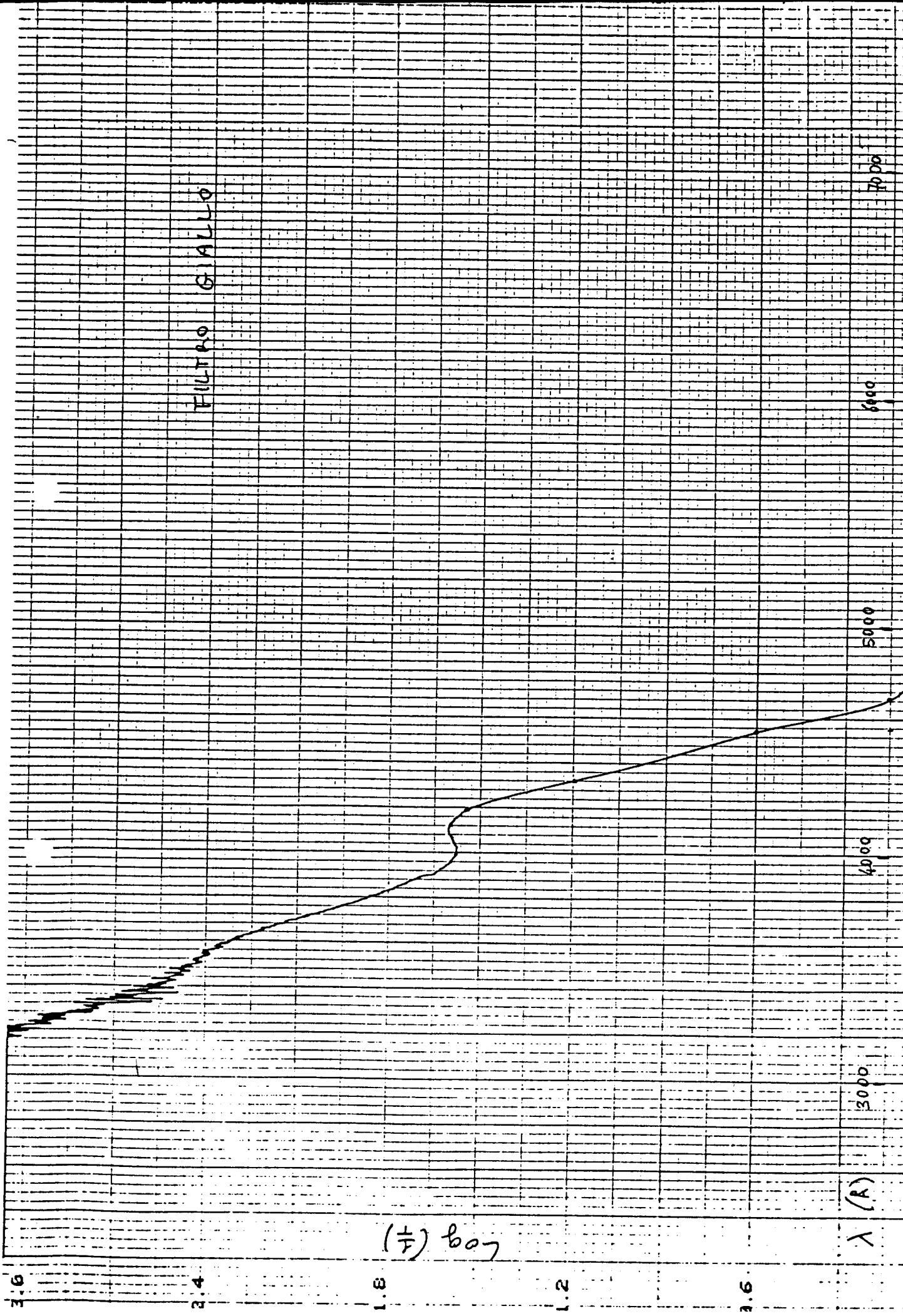
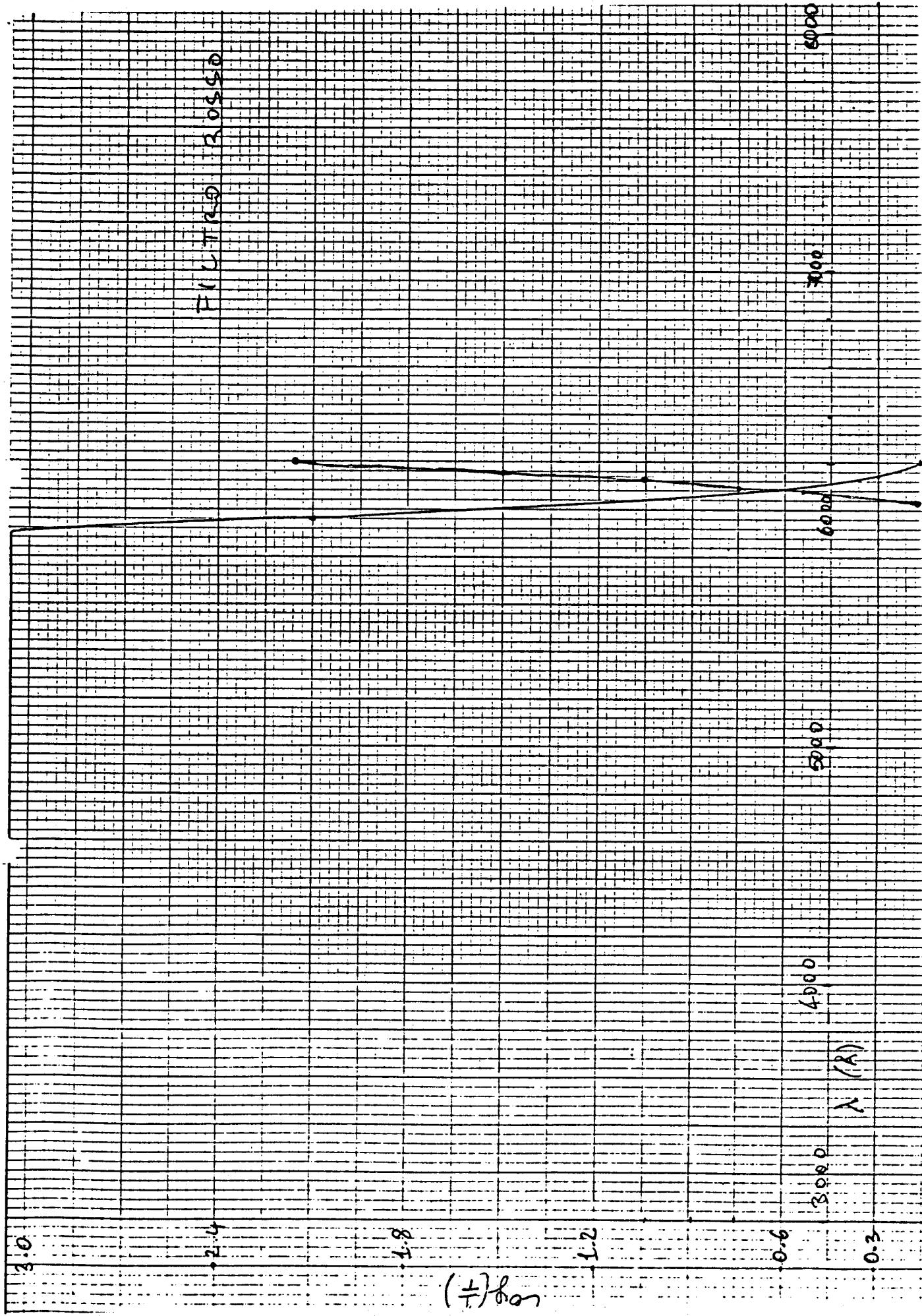


FIGURE C 2200









7000

6000

5000

4000

3000

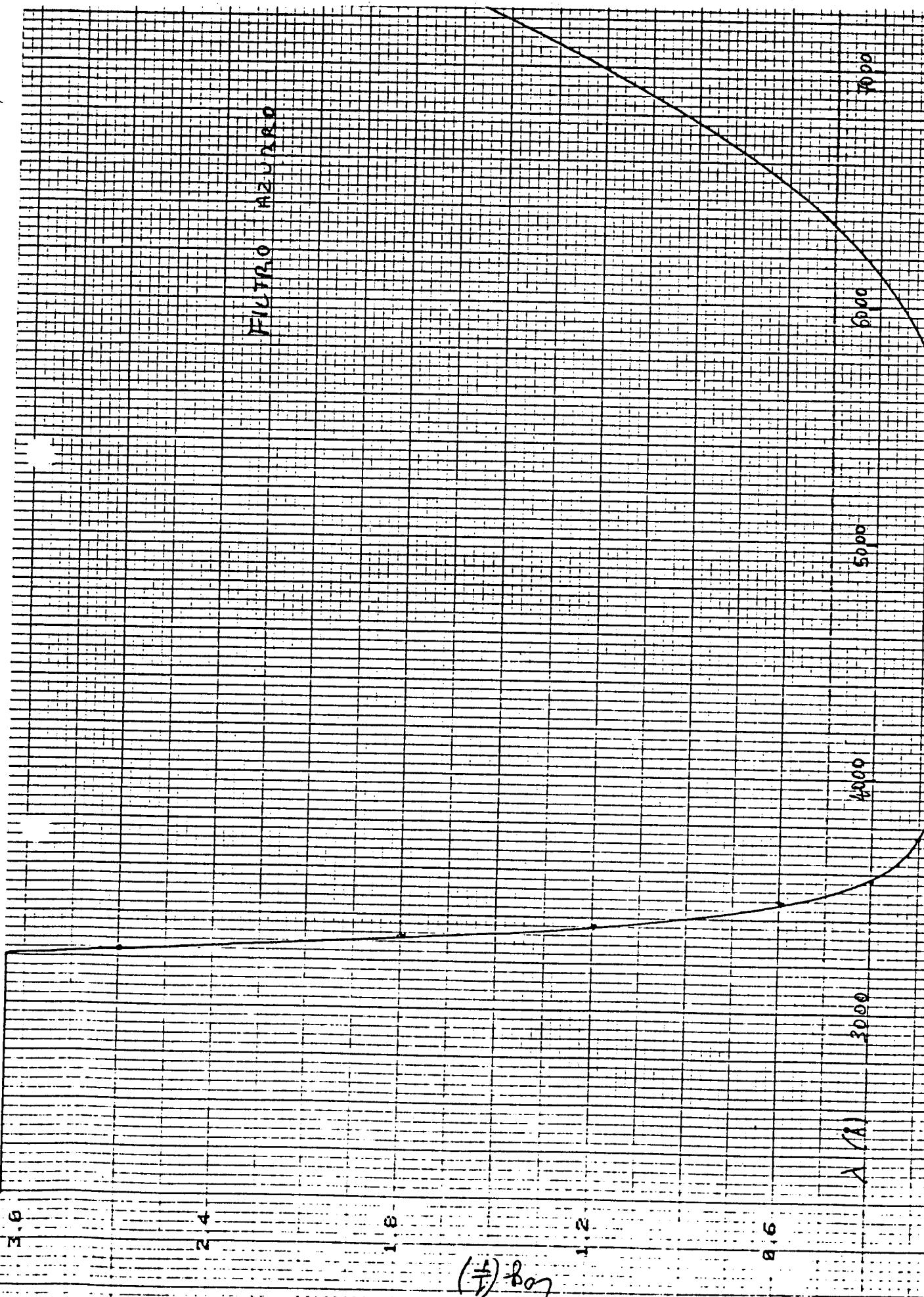
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1000

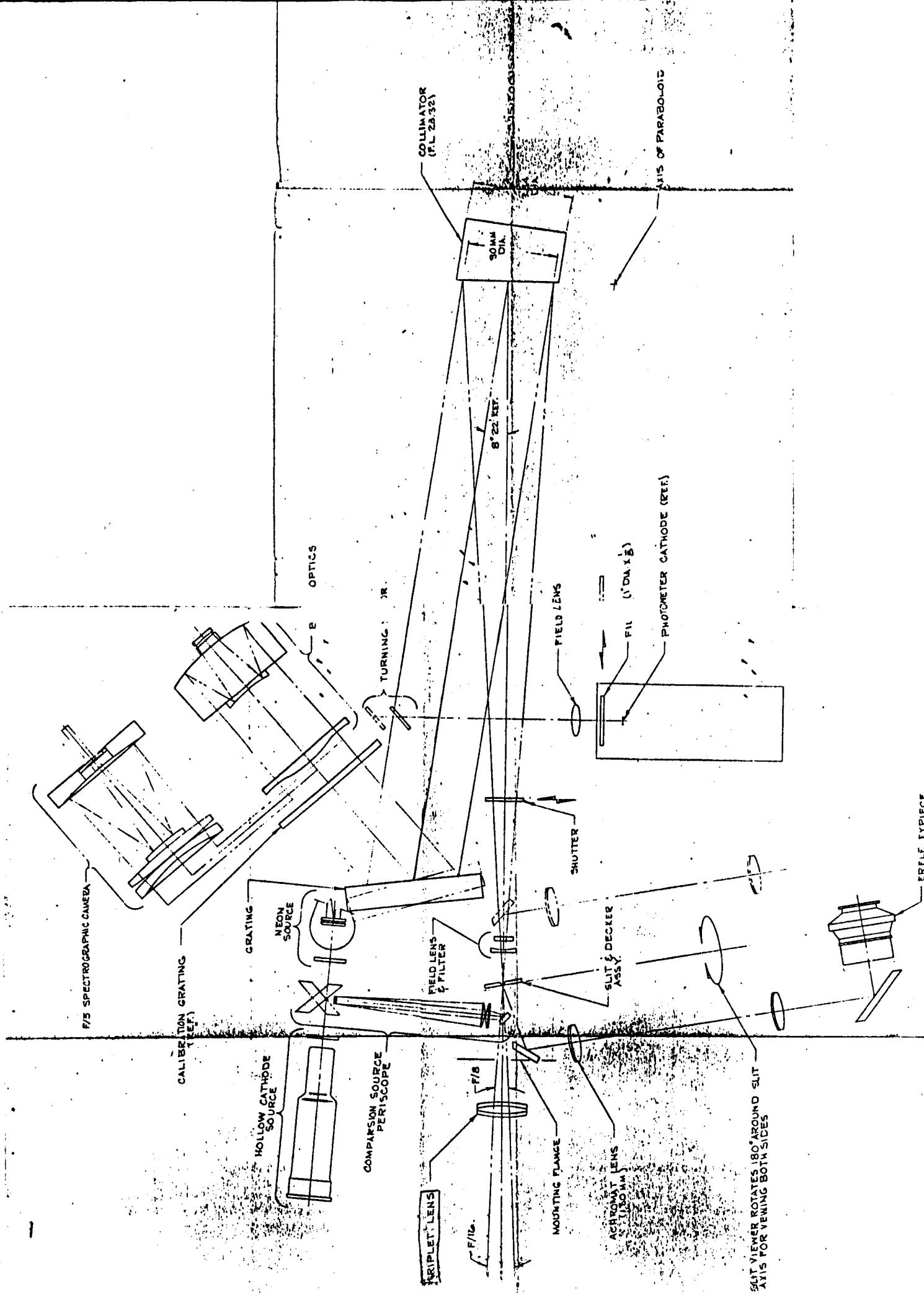
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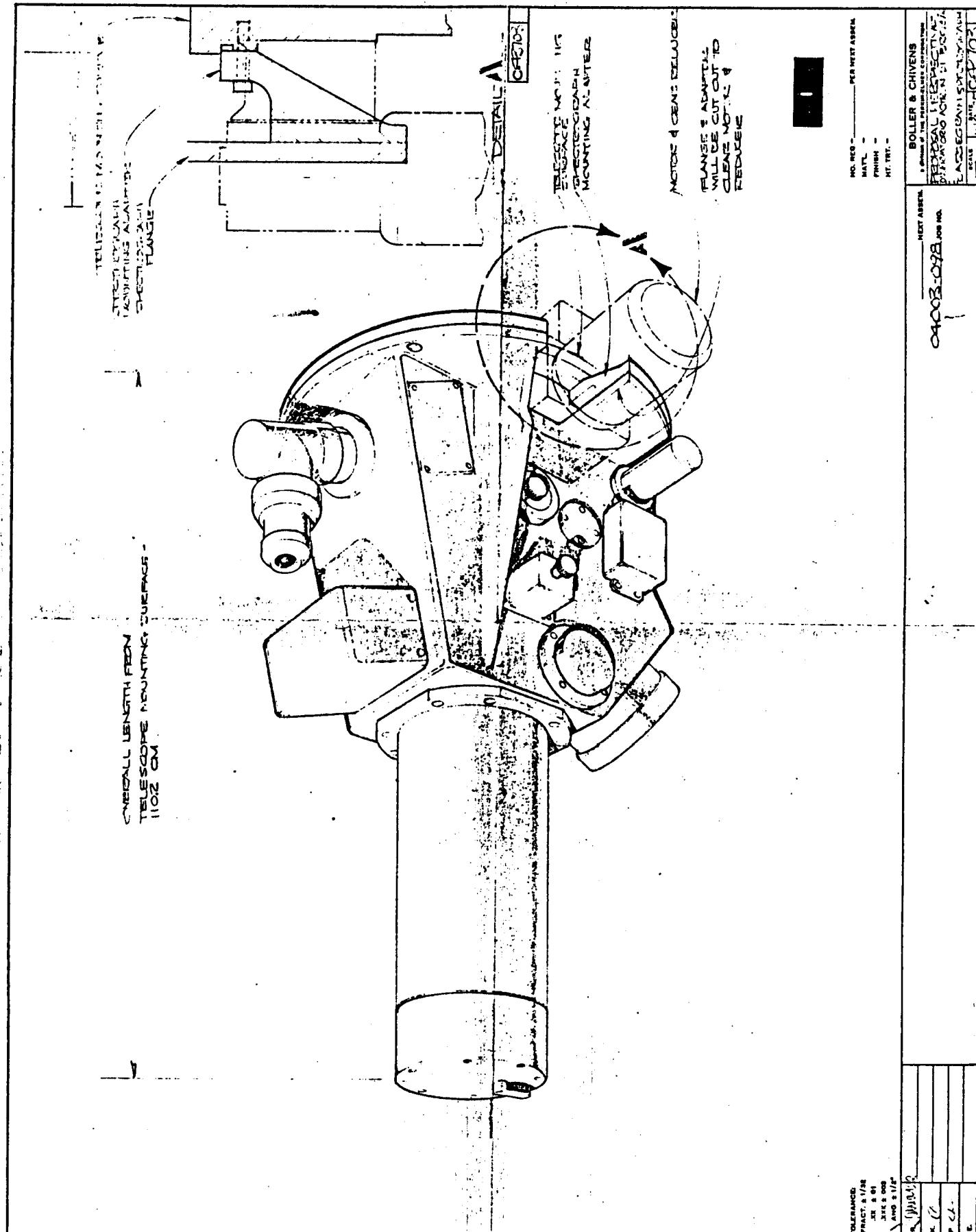
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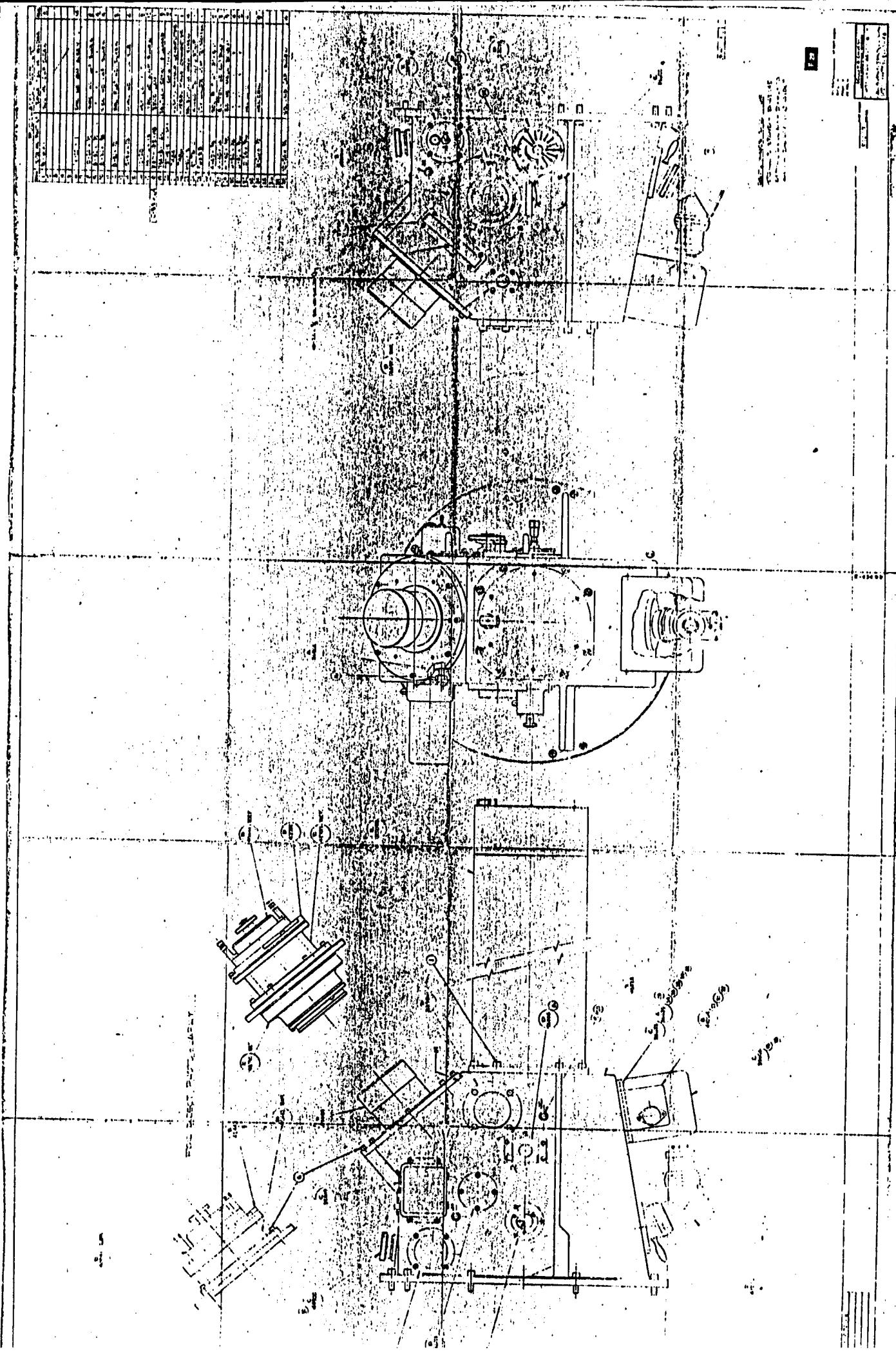
FILTRO AZUARO

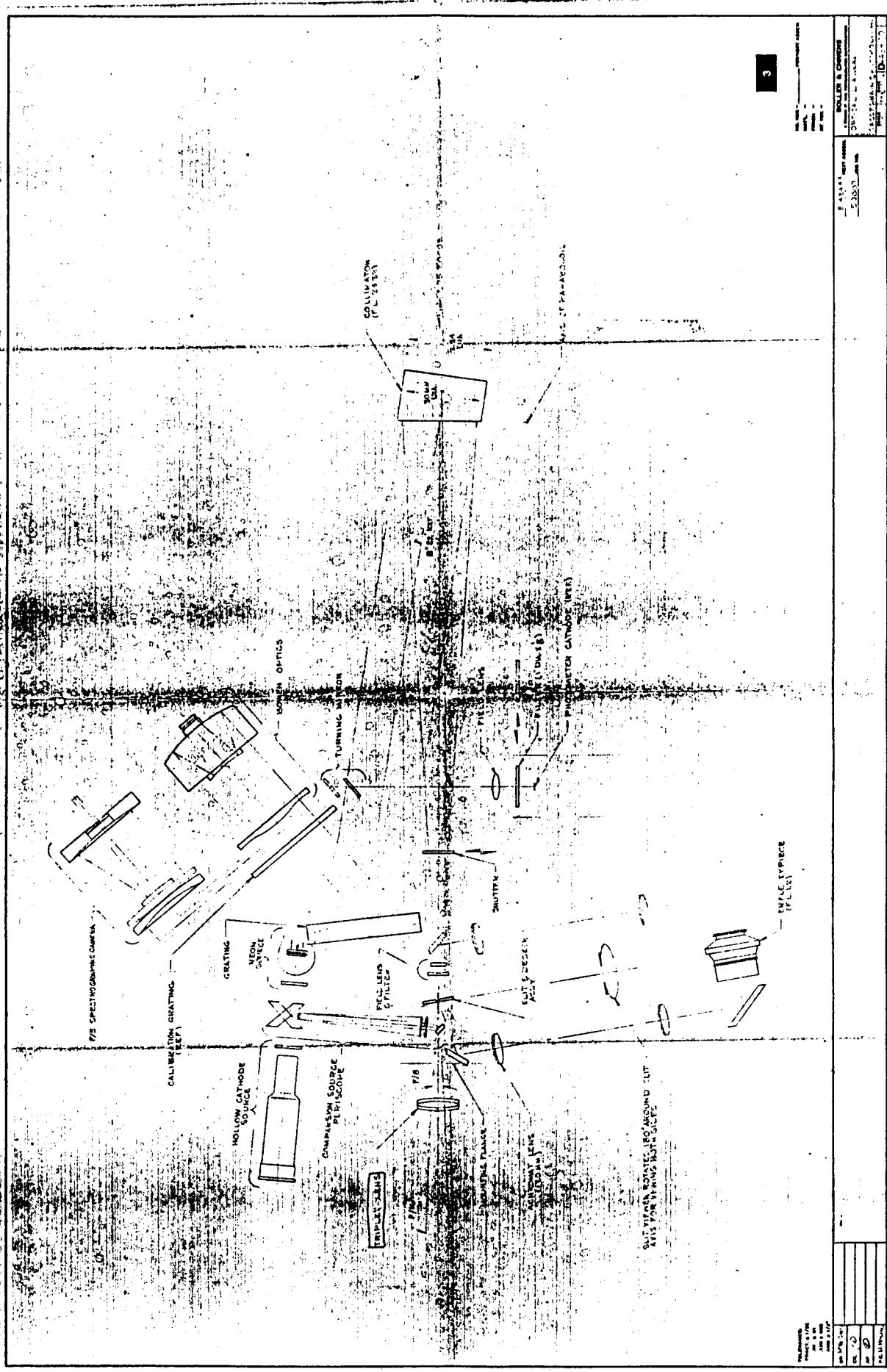


- 1) VISIONE PROSPETTICA
- 2) VISTA D'ASSIEME
- 3) SCHEMA OTTICO
- 4) SCHEMA ELETTRICO GENERALE
- 5) CAMERA FOTOGRAFICA F/5
- 6) MODULO PER FOTOGRAFIA DIRETTA CAMERA F/5
- 7) CAMERA FOTOGRAFICA CORTA (Bowen optics)
- 8) MODULO PER FOTOGRAFIA DIRETTA CAMERA CORTA
- 9) COLLIMATORE
- 10) GRUPPO PORTA RETICOLO
- 11) CONVERTITORE DI FOCALE
- 12) GRUPPO PORTA FILTRO E SPECCHIETTO
- 13) VISORE DI FENDITURA
- 14) GRUPPO PER L'ILLUMINAZIONE DELLA FENDITURA
- 15) GRUPPO FENDITURA
- 16) ESPOSIMETRO
- 17) PORTALASTRE
- 18) OTTURATORE
- 19) LAMPADA HOLLOW CATHODE (lampada ferro)
- 20) LAMPADA AL NEON
- 21) SCHEMA ELETTRICO ALIMENTAZIONE LAMPADE
- 22) CARRELLO DI SOSTEGNO DELLO SPETTROGRAFO
- 23) FLANGIA DI ATTACCO DELLO SPETTROGRAFO
- 24) ADATTATORE PER LA FLANGIA D'ATTACCO



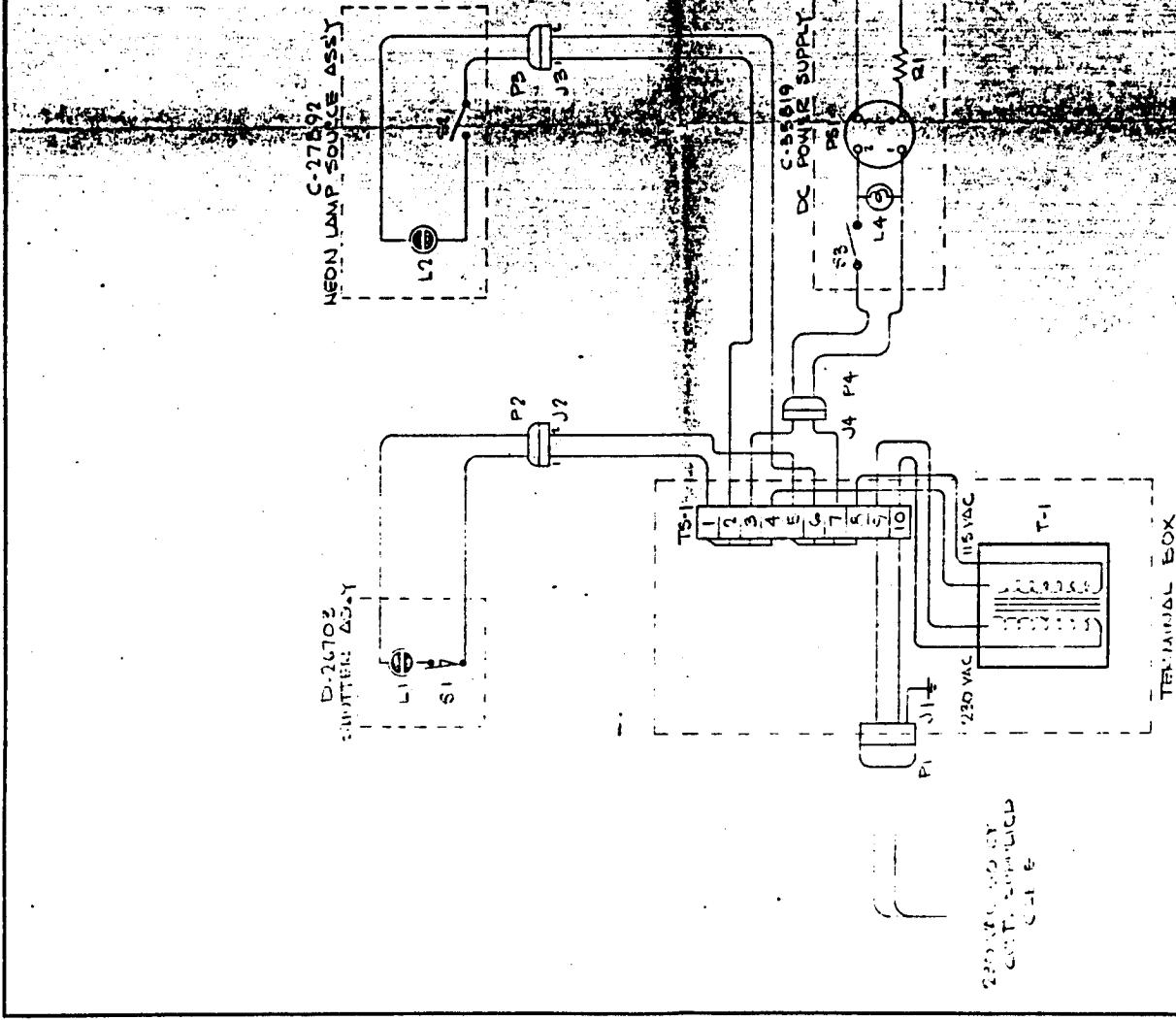






POULINING E. PLATE		L127
ITEM PART NUMBER	DESCRIPTION	
P1	7404	WIRE TWIST LOC CONNECTION
J1	7405	" INLET
P2, P3, P4	754-3-303N	DEUTCH BULKHEAD CONN.
J2, J3, J4	757-3N-059	CABLE CONN.
T51	37-TD1	KOLKA TERMINAL STRIP
J5	PC-5-B	POSITION ELECTRONICS CATALOG SEC.
T5	PC-5-B3	TRY ON STEP DOWN TRANSFORMER
P51	44-400	FEEDTHROUGH 1C HAMMER SWITC
H1	NL-722611	WEIGHT CHRONIC VOLUNTARY TIME
L1	NE-40	DIAL GO LEON CAP
L2	5A-7512-0135-302	NEON LAMP
L3	477-8836-0921	SHIMU LEADS CAP ASSY
L4	756	" "
R2	CLUST21	OMNIATE LEVELATOR (12N-11K)
S1	15MA1	TRIM POT (2V15R-100K)
S2	8391-K7	MICROSWITCH LIMIT SWITCH
S3	S11TS1-2	CUTTER HAMMER TOGGLE SWITCH
		MICROSWITCH LIMIT SWITCH

C-417x5

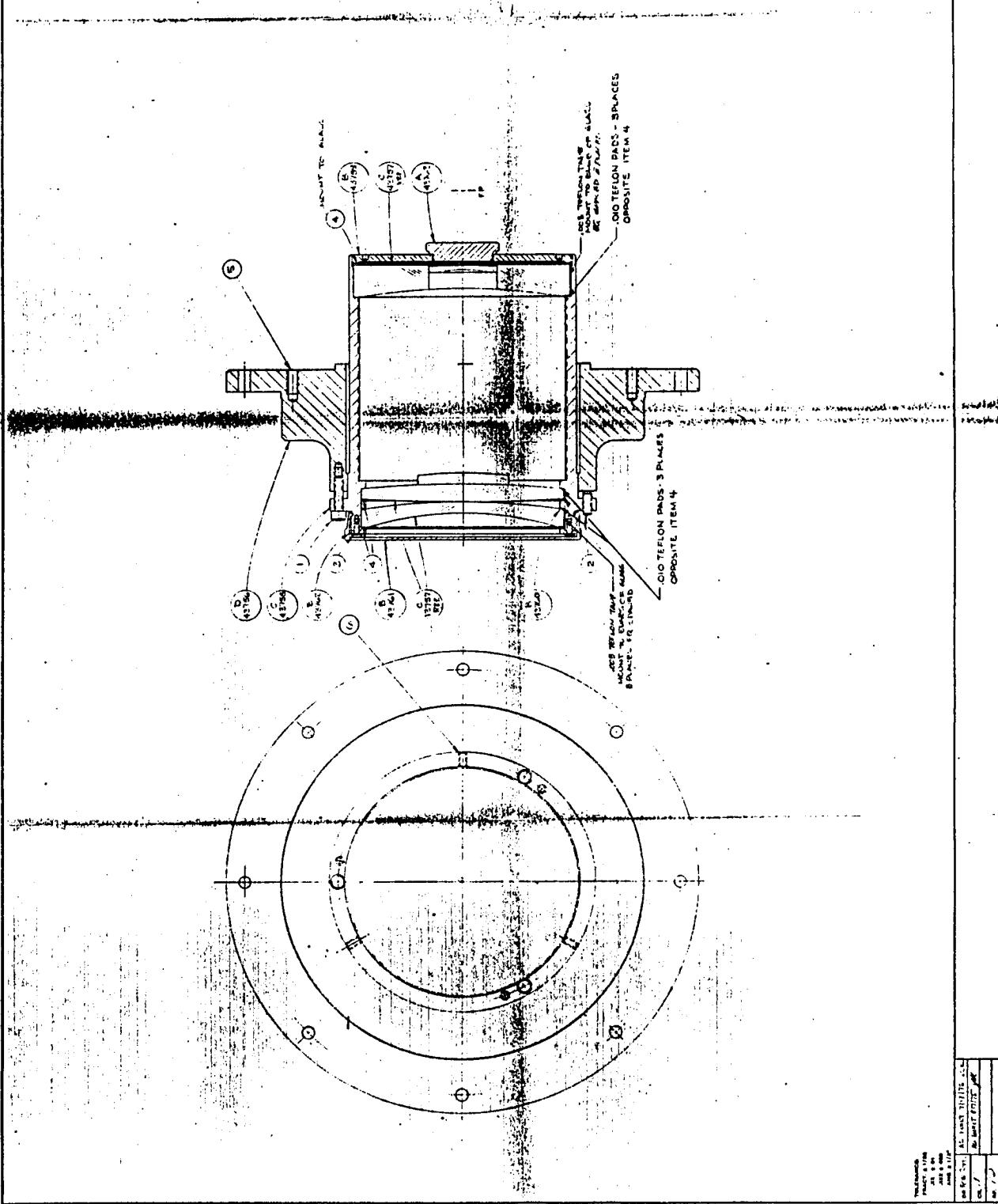


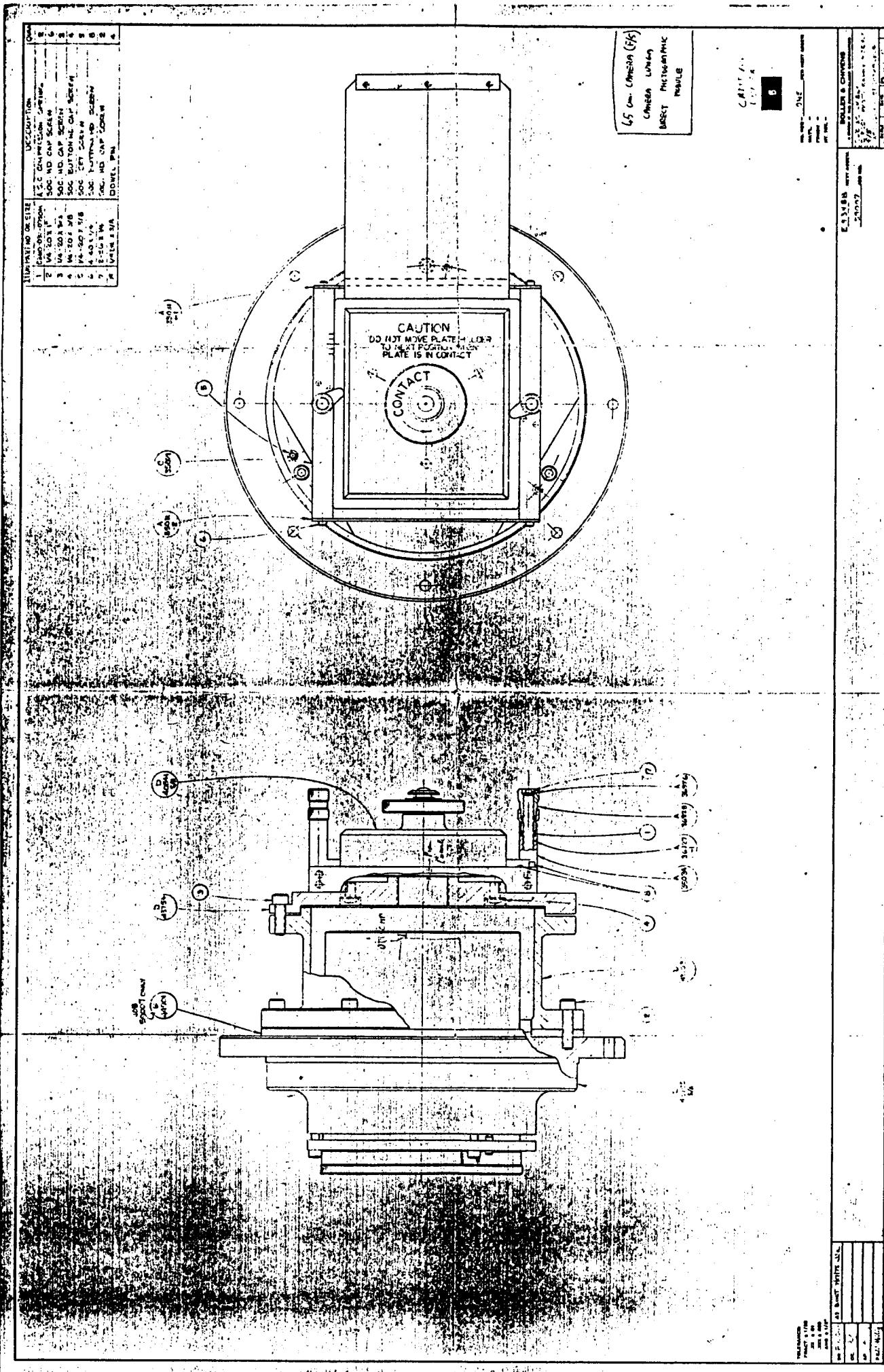
- 4 094 - Next Anew	
5-27171-C Job No.	
ROLLER & CHIVENS • <small>WE ARE THE LEADERS IN THE INDUSTRY</small> • <small>WE ARE THE LEADERS IN THE INDUSTRY</small>	
NO. 100 - LEE - OUR NEXT ANEW MATH - FISHIN - HT. TAT. - C. C. - ORGAN - DANCE - GOLF - C. C. - DANCE - GOLF -	

E 43488 E
59007

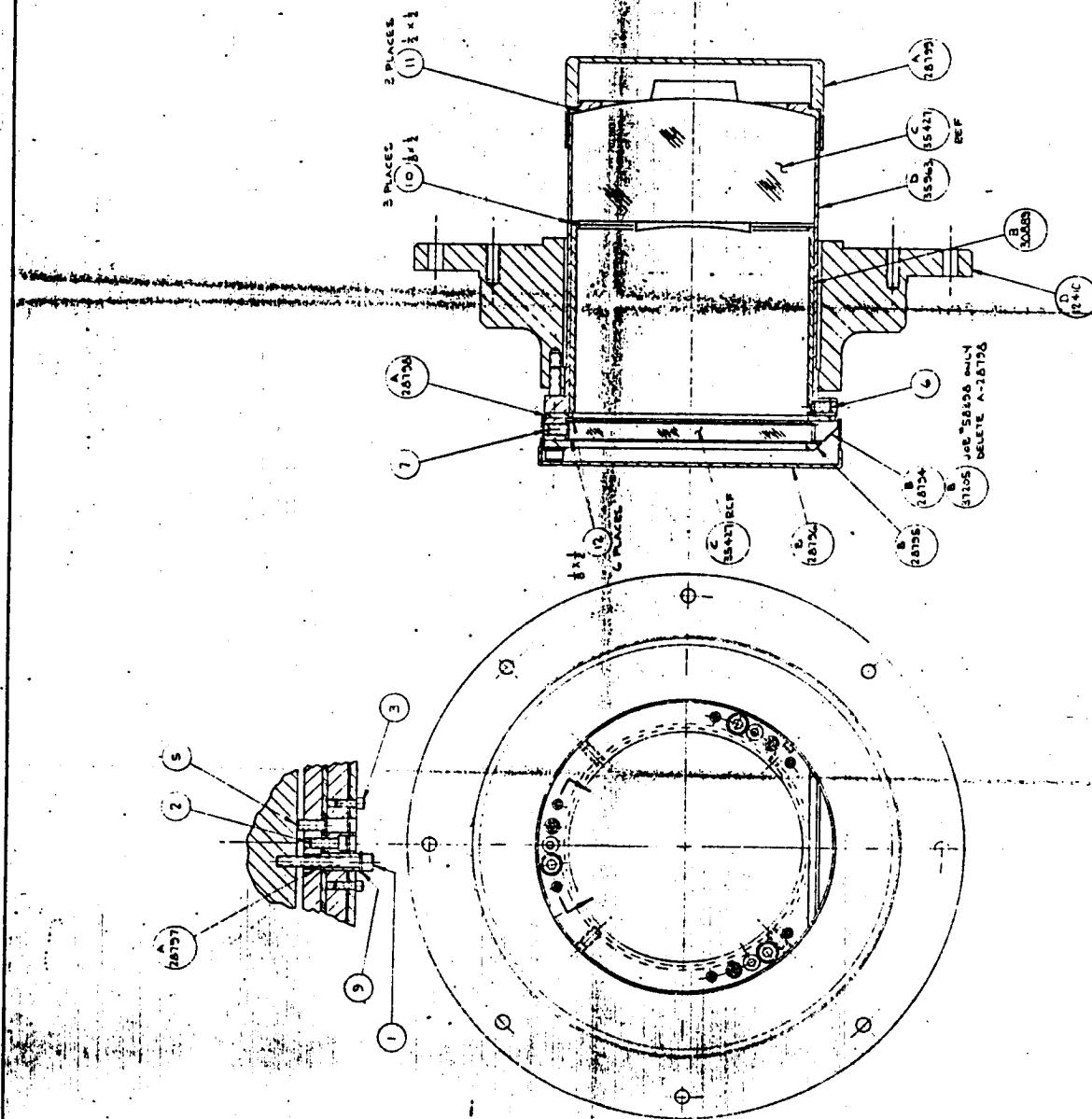
1

FACT. A 1/32	
JIN ± 91	
JIN ± 009	
ANG ± 1/2°	
DE 12C	
CK W Holes	
AP ✓	
PC ✓	



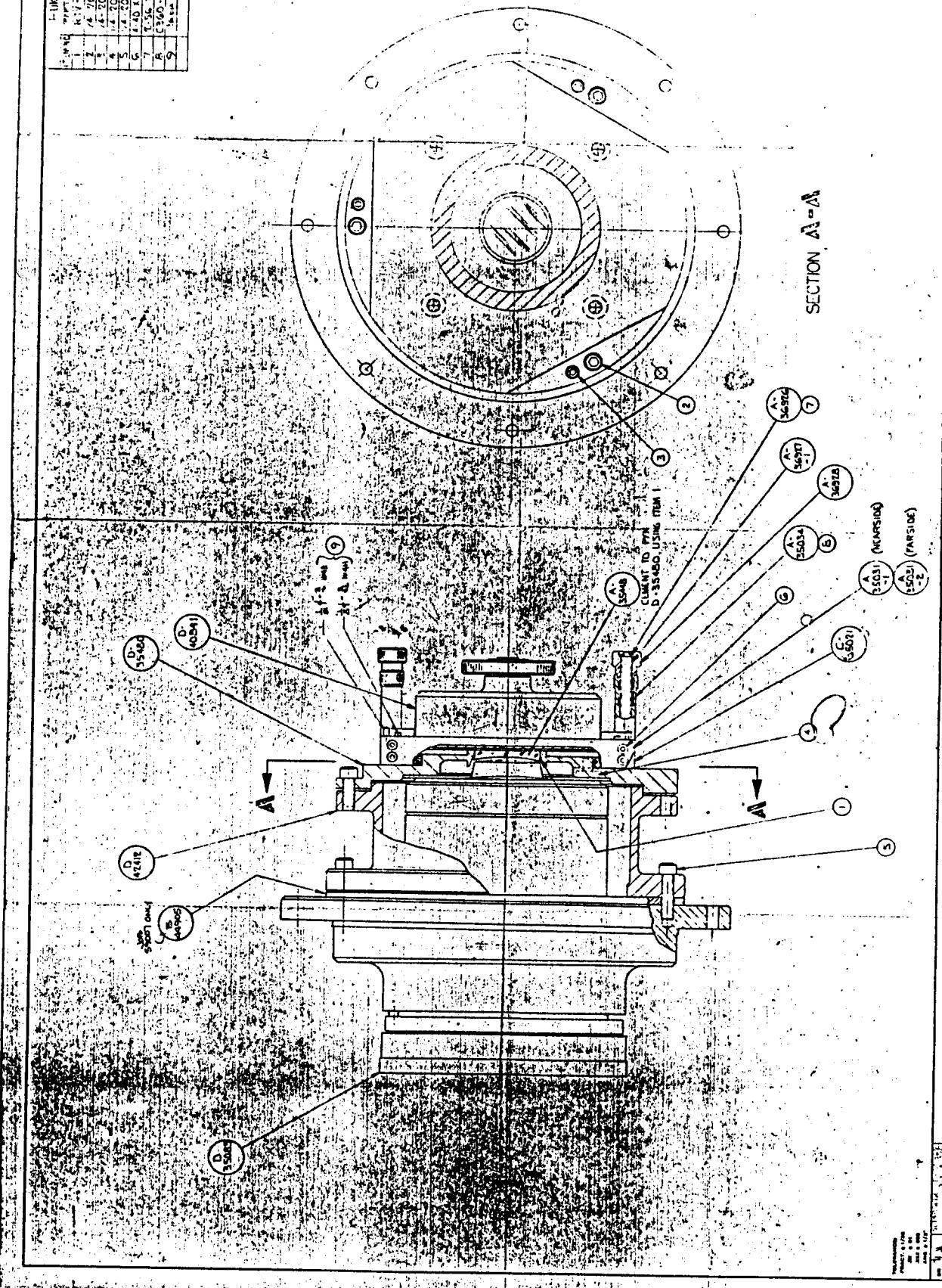


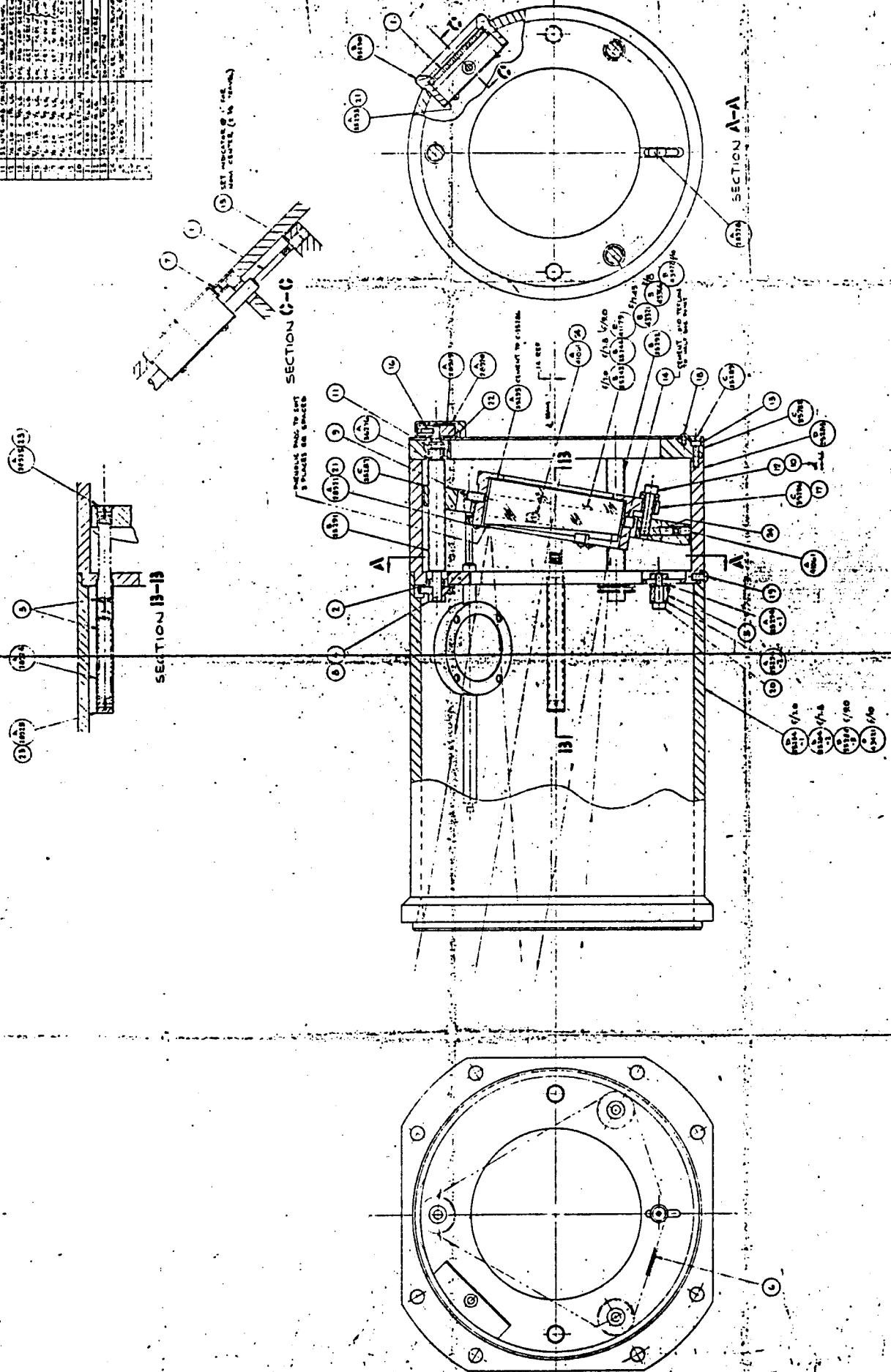
34 cm. (optical) (F/L_0)
 (optical) 11.479
 optics module

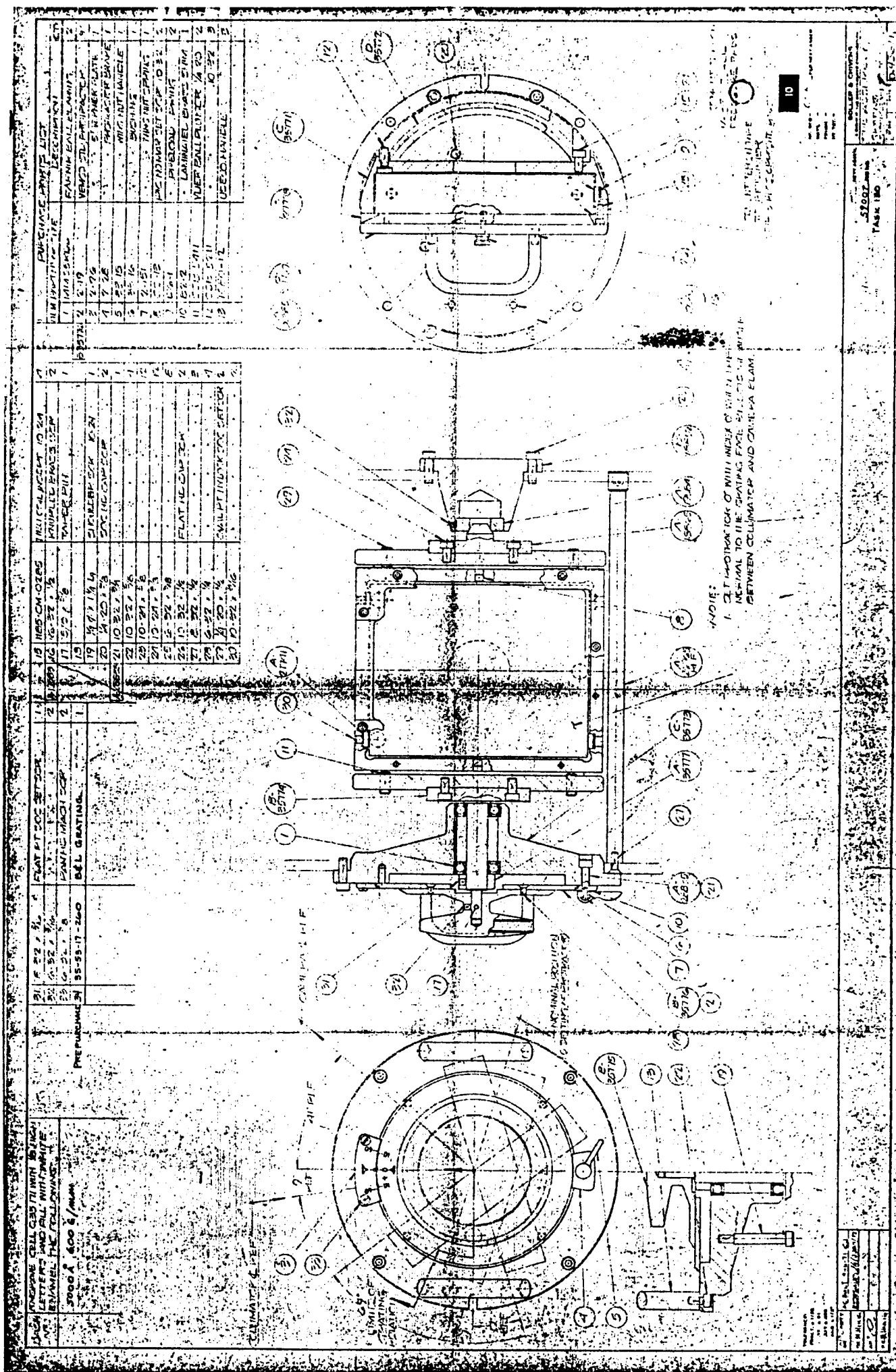


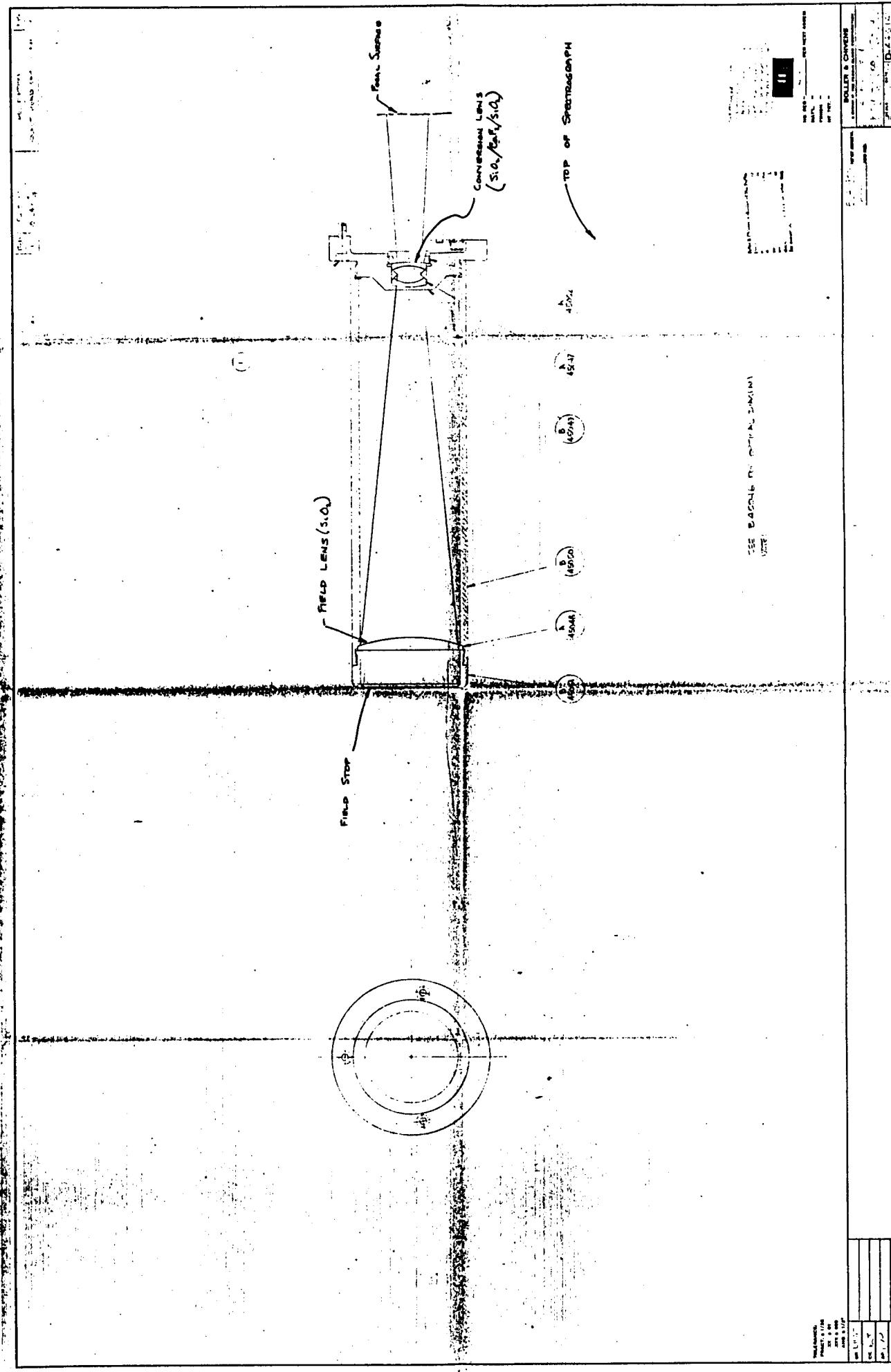
سیاه و سفید

T-1000001 PARTS LIST	
ITEM NO.	DESCRIPTION
1	KIT-1000001
2	1/4" 10-32 SCREW
3	1/4" 10-32 SCREW
4	1/4" 10-32 SCREW
5	1/4" 10-32 SCREW
6	1/4" 10-32 SCREW
7	1/4" 10-32 SCREW
8	1/4" 10-32 SCREW
9	1/4" 10-32 SCREW





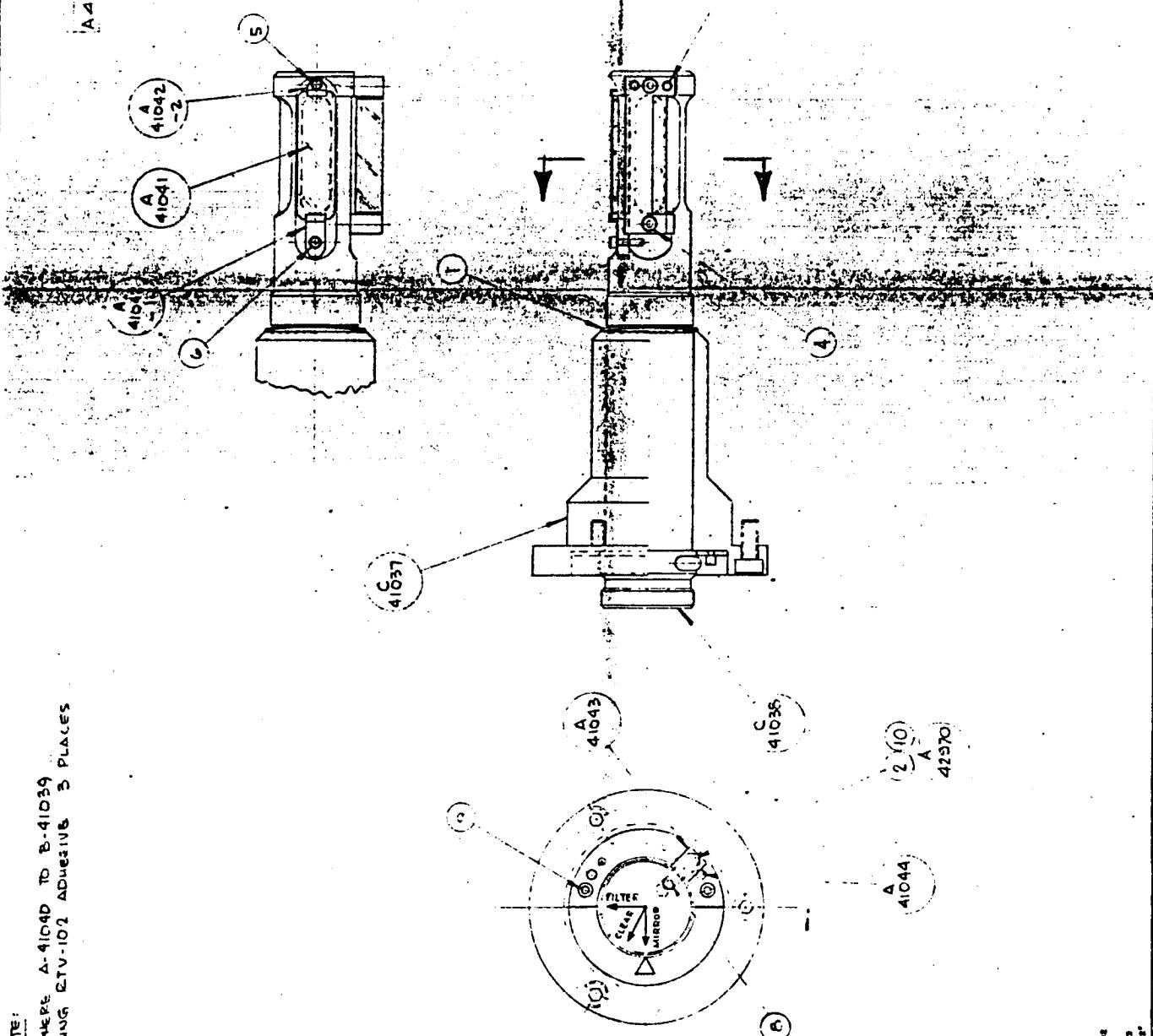




NOTE:

▲ ACHIEVE A-4104D TO B-41039
USING RTV-102 ADJUSTING 3 PLACES

PURCHASE PARTS LIST	
ITEM	Part # - S/N# DESCRIPTION OR VENDOR
1	5100-112 TUBE - EXTERNAL DRAIN
2	SSBL-54N VILOC - BALL VALVE - (1-10)
3	4-40x 1/4 SOC. SET SCR. FLAT 13T.
4	4-40x 3/8 SOC. HD CAP SCREW
5	2-56x 1/2 SOC. HD CAP SCREW
6	2-56x 3/8 SOC. HD CAP SCREW
7	8-32x 5/8 SOC. SET SCR. CUP PT.
8	9-40x 1/4 SOC. HD CN SCREW
9	10-32x 5/8 SOC. SET SCR. CUP PT.



TOLERANCE:
PRACT. ± 1/16
.005 ± .003
.005 ± .003

NO PEE - C-15 - PERMIT ASSEM.
MATERIAL -
FINISH -
HT TYP. -

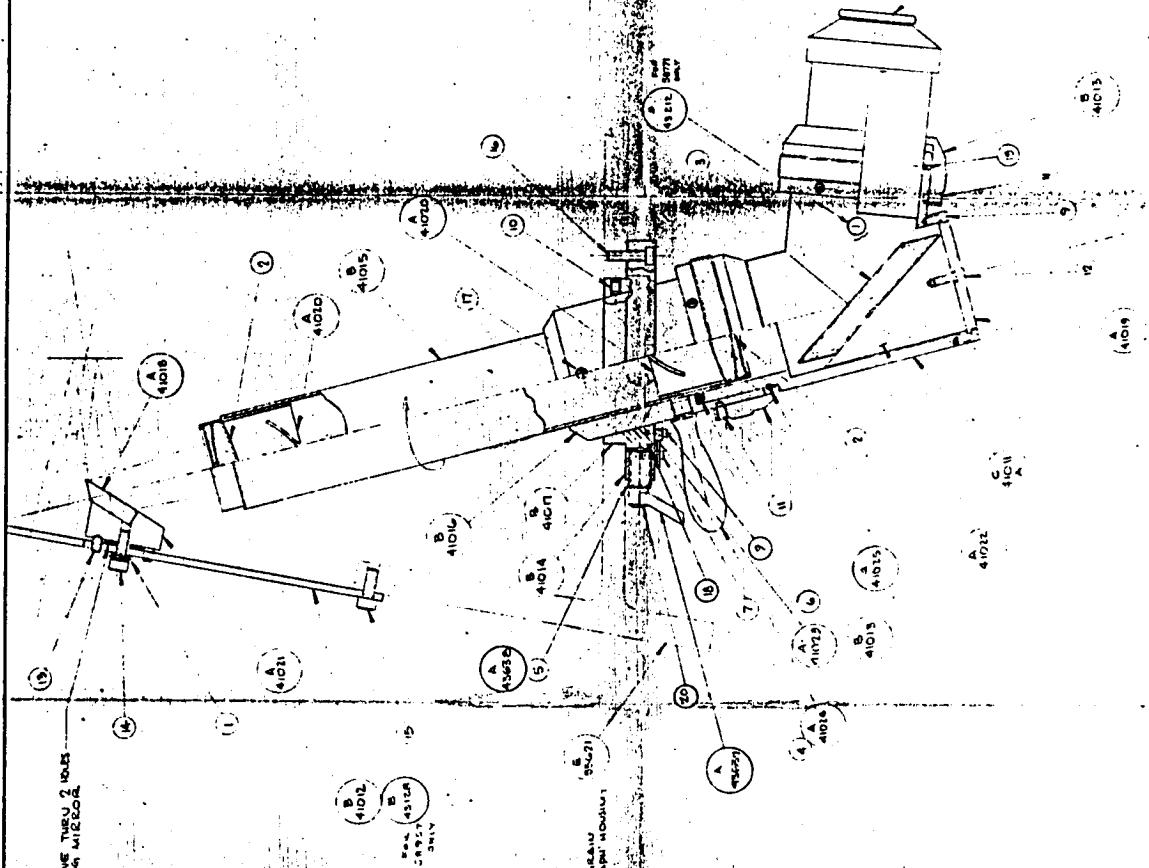
12

BOLLER & CHIVERS
DIVISION OF THE PRECISION MANUFACTURERS CORPORATION
S-115 - L-512-A-101
FILTERS - AIR FILTERS
C-41024 - FILTER HOUSINGS
C-41025 - FILTER HOUSINGS
C-41026 - FILTER HOUSINGS
C-41027 - FILTER HOUSINGS

E-4014A - MFG. ASSM.
59007, S/N 1111, 58770
JOB NO.

PLASTIC ADHESIVE THRU 2 HOLES
AFTER ALIGNING MIRROR.

PURCHASE PARTS LIST



VIEW A-A

VIEW B-B

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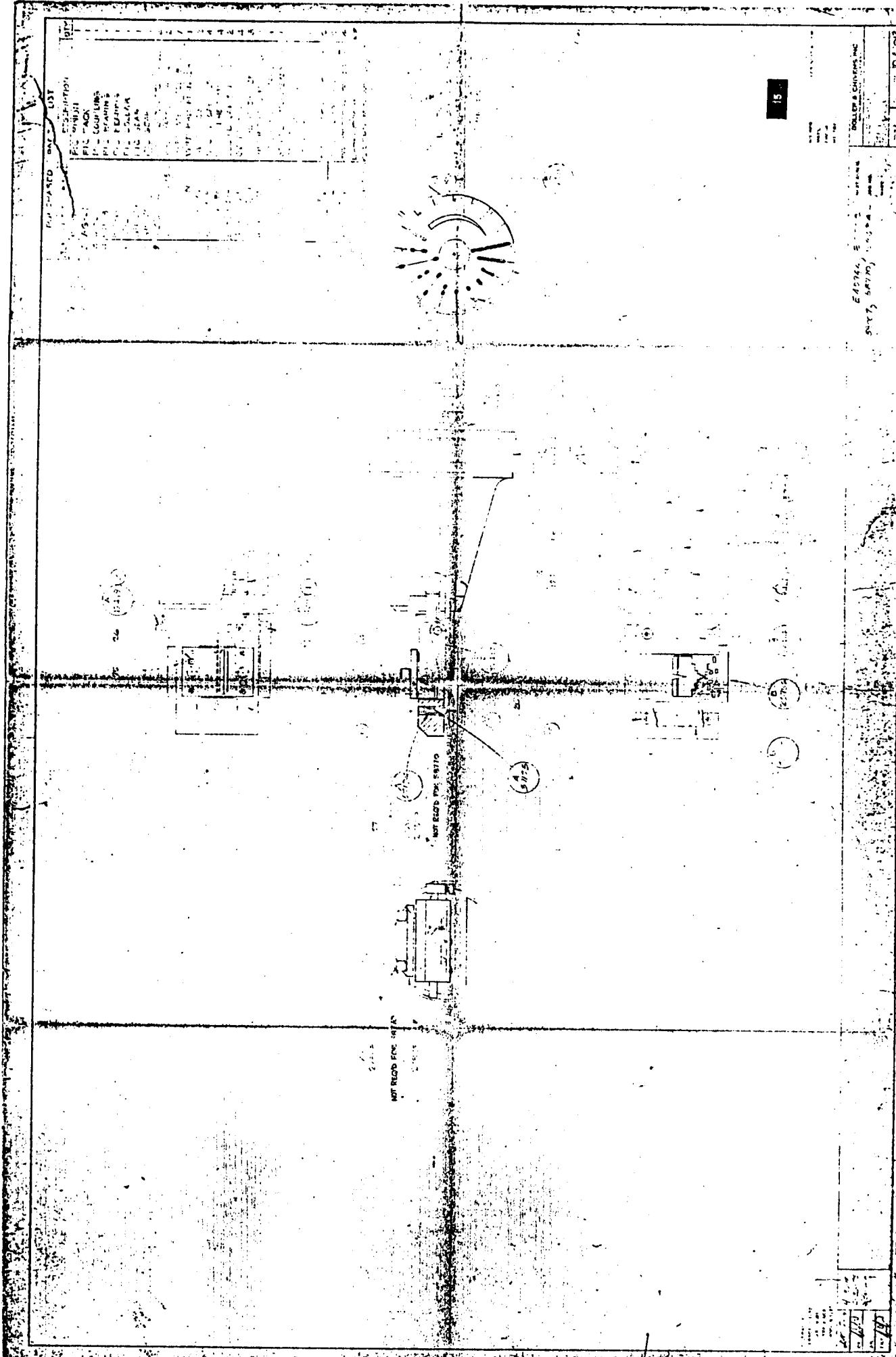
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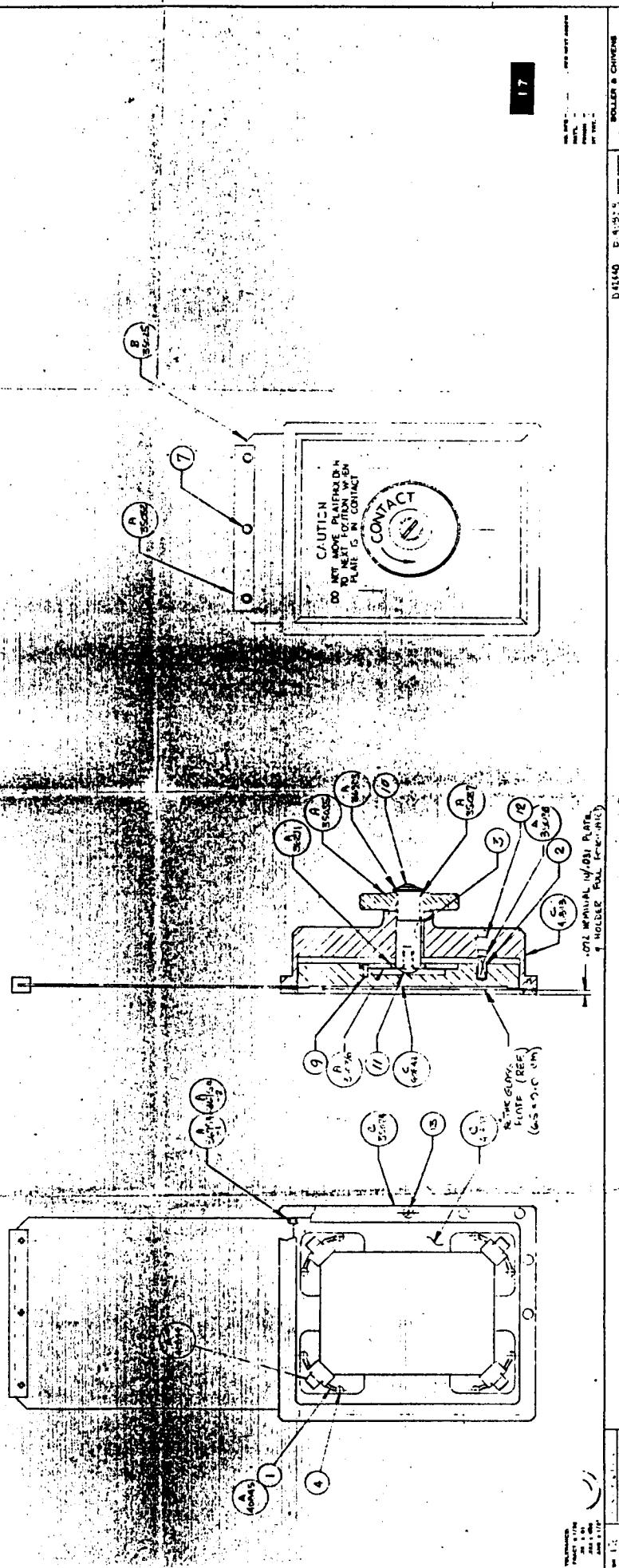
B

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Purchased Parts			
Ref	P/N	Size	Metric
1	203 S-1100	CHASSIS	CARRIER STANCHION
2	0150-018-072M (REINFORCED)	AIR BOX CAGE	ARMED CARRIER AND AIR BOX
3	3/8 x 1"		WHEELCROWN KEY
4	2.56 x 1/8		SCREW NO CAP (SLOAN)
5			
6			
7	2.56 x 1/8		SCREW NO CAP SC
8			
9	.05-.07 x 3/16		PUNCH HOLE SIZE
10	.10-.32 x 1/8		PUNCH HOLE SIZE
11	.10-.32 x 3/16		PUNCH HOLE SIZE
12	1/2 x 10 x 1/8		FUR PT SET SC
13	1/2 x 10 x 3/16		FUR PT HOLE SC
14			
15			



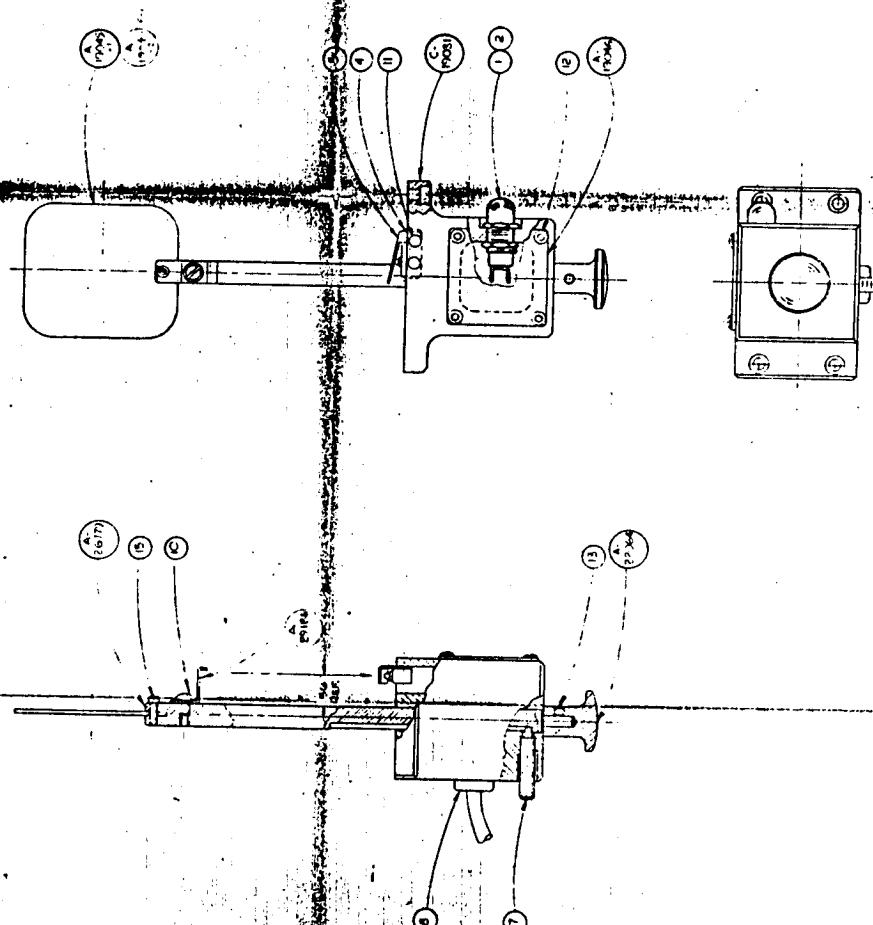
Part No.	Description	Quantity	Unit
51447	DIA 100 E-10125	1	PC
58770	SPRING	1	PC
	ROLLER & CHAIN	1	PC
	CONTACT	1	PC
	PLATE	1	PC
	WHEEL	1	PC

18
MAY 1967
RECEIVED
BY
FBI - NEW YORK

59-607-1931-4-5-407

SEARCHED
INDEXED
SERIALIZED
FILED
FBI - NEW YORK

ITEM	ITEM NO. OR REF.	PURCHASED PARTS LIST DESCRIPTION
1	HF-1C	DATA CARD
2	37-125-0001-A	WIRE, TIN & NICKEL 1/16" X 1/2" X 10 FT.
3	715-1-514-C	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
4	15A1	WIRE, TIN & NICKEL, 1/16" X 1/2" X 10 FT.
5	15-2	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
6	15-3	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
7	15-4	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
8	15-5	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
9	15-6	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
10	15-7	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
11	4-1-6-12	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
12	10-1	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
13	10-2	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
14	10-3	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
15	10-4	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
16	10-5	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)
17	10-6	FLAT HEAD SCREW, 1/4-20 X 1/2" (100)

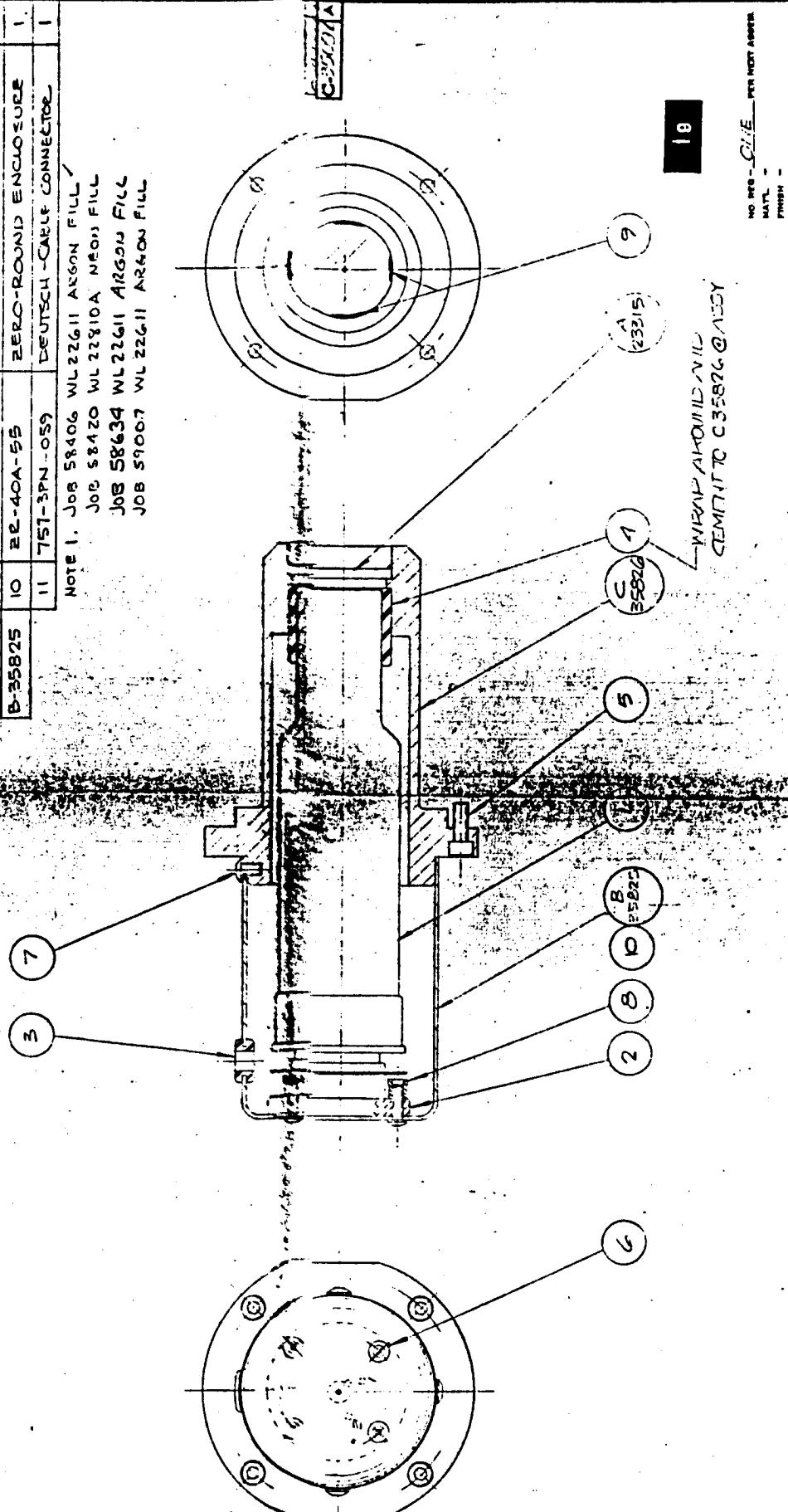


SEARCHED	INDEXED
SERIALIZED	FILED
APR 24 1967	
FBI - NEW YORK	

LURCHUSIF PARTS LIST

ITEM	PART NO. OR SIZE	DESCRIPTION	QTY
1	SEE NOTE 1	WELTING/PIPE 11/16" O.D. X 12' FT	1
2	N° X5-B	MONOVA ELECTRONIC OPEN SOC.	1
3	N° 5	RUBBER REFLAT GASKET	1
4	3/8" x 1" x 6"	MONOLIC RUBBER	1
5	10-27 x 1/2"	SOC 11/16" C.R.P. S.C.H.	1
6	6-32 x 1/2"	SOC BUTTON HD SCRE	4
7	8-32 x 1/4"	SOC BUTTON HD SCRE	4
8	G-3/2	ALLENUT	4
9	RTV 102	G.E. SILICONE ADHESIVE	A/R
10	E22-40A-55	ZERO-ROUND ENCLOSURE	1
11	751-3PN-059	DEUTECH -CABLE CONNECTOR	1

NOTE 1. JOB 58406 WL22611 ARGON FILL
 JOB 58420 WL22810A NEON FILL
 JOB 58634 WL22611 ARGON FILL
 JOB 59007 WL22611 ARGON FILL



NO. 1000-C-7000 PER MONT AREA
 MATTL -
 PHASE -
 HT. THT. -

WIRE & ALUMINUM
 CEM717TC C35826 @ 100%

TOLERANCES
 TRACT. A 1/32
 AX. 0.01
 RAD. 0.005
 CEM717TC A 1/32 0.005
 AX. 0.01
 RAD. 0.005

60° COUNTER AS BUILT 9.14-71 C.I.
 CEM717TC A 1/32 0.005
 AX. 0.01
 RAD. 0.005
 AX. 0.01
 RAD. 0.005

E-13922

59007, 58771, 58634

58107, 58420

58406, 58634

BOLLER & CHIVENS
 A Division of The International Telephone & Telegraph Corporation
 1000 CEM717TC C35826 @ 100%
 1/32 0.005

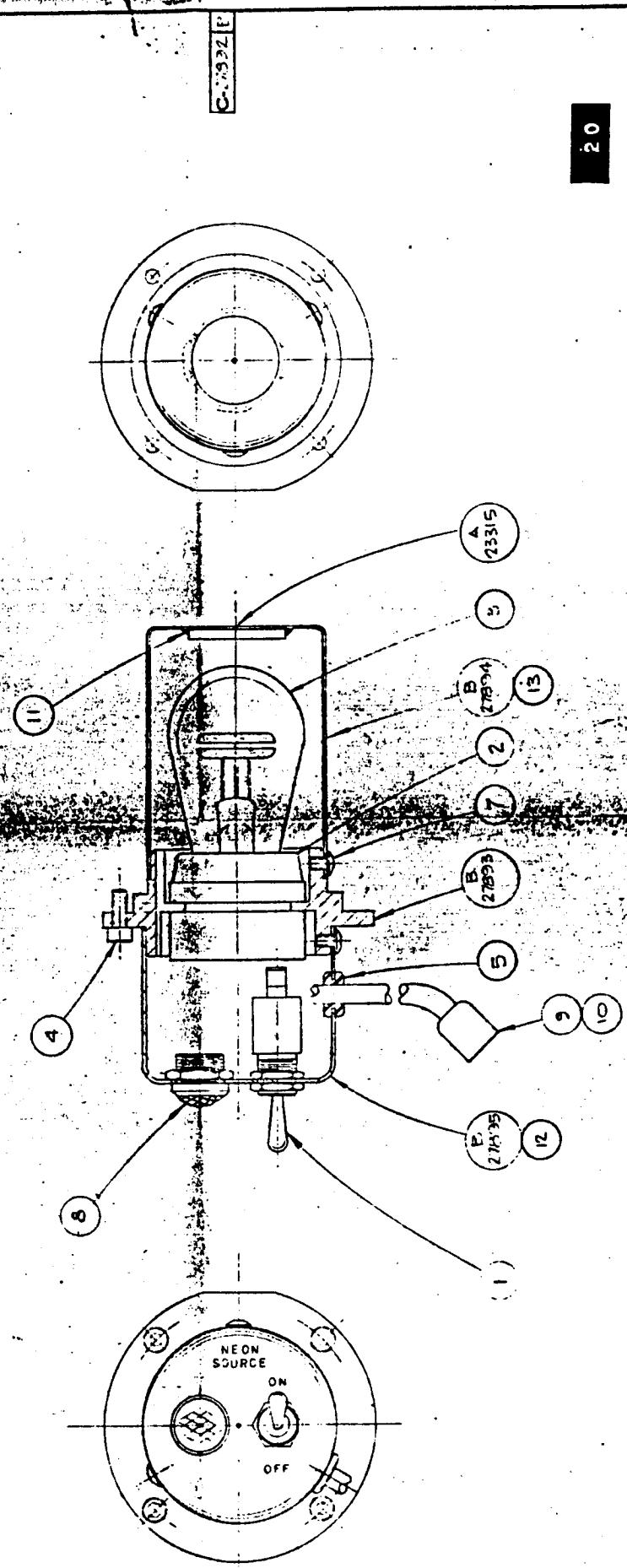
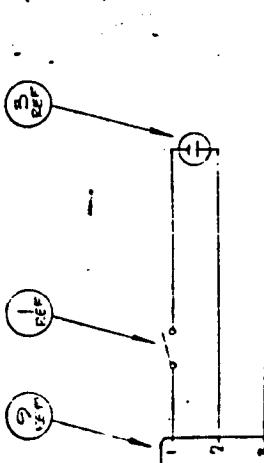
58406, 58634

PURCHASED PARTS LIST

ITEM	PT. NO OR SIZE	DESCRIPTION	QTY
1	8391K7	CUTLER HAMMER TUGGLE SWITCH	1
2	*400	EDWARD MED BASE LAMP SOCKET	1
3	NE-140	GE NEON LAMP	1
4	*10 21 x 1/2	1/2 IN. C.R. SCREW	4
5	*5	RUBBER CRAFT GROMMET	1
6			
7	*6 32 x 1/4	1/4" BUTTON HD SCREW	6
8	514-2512-0435-302	LILCO LENS CAP ASSY	1
9	1513-CM1-059	BLUETT-H CABLE CONNECTOR	1
10	12501	ALPHA CABLE	1
11	ETV 102	12.5 VOLT 15 C. ALIC SOURCE	1
12	ZR-40A-32	2000 MFa - SOUND ENVELOPE	1
13	ZTR-37A-52	" " "	1

ELECTRICAL SCHEMATIC

177



NO. REC. — PER UNIT ASSEMBLY
MATERIAL —
FINISH —
INT. TYP. —

BOILER & CHIMNEY
A Division of The International Corporation
LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

NO. REC. — PER UNIT ASSEMBLY
MATERIAL —
FINISH —
INT. TYP. —

BOILER & CHIMNEY
A Division of The International Corporation
LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

NO. REC. — PER UNIT ASSEMBLY
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LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

NO. REC. — PER UNIT ASSEMBLY
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INT. TYP. —

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LAMP ASSEMBLY
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CABLE CONNECTOR
F-10001 10001 C-73321P

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FINISH —
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A Division of The International Corporation
LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

NO. REC. — PER UNIT ASSEMBLY
MATERIAL —
FINISH —
INT. TYP. —

BOILER & CHIMNEY
A Division of The International Corporation
LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

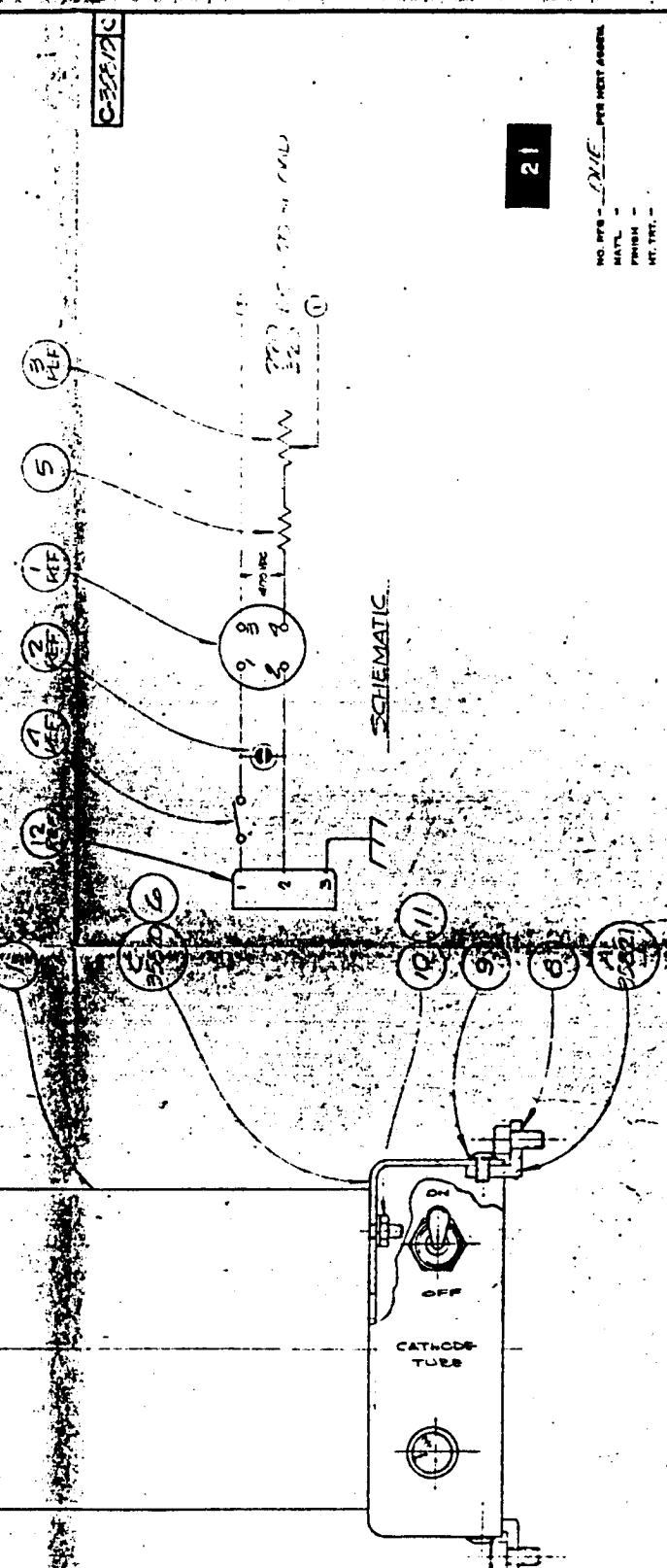
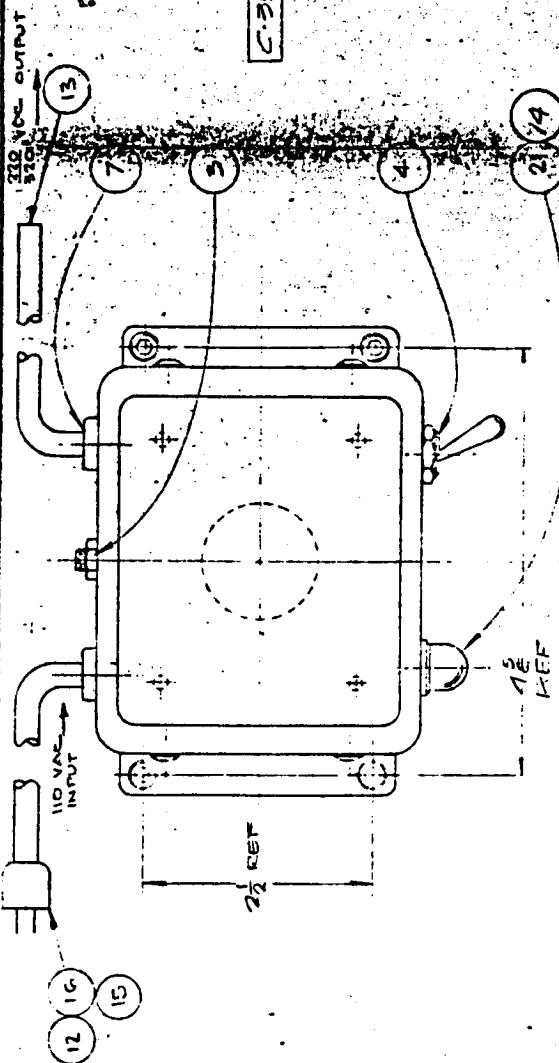
NO. REC. — PER UNIT ASSEMBLY
MATERIAL —
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BOILER & CHIMNEY
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LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

NO. REC. — PER UNIT ASSEMBLY
MATERIAL —
FINISH —
INT. TYP. —

BOILER & CHIMNEY
A Division of The International Corporation
LAMP ASSEMBLY
INTEGRAL LAMP SOURCE
CABLE CONNECTOR
F-10001 10001 C-73321P

FUNCTIONAL PART LIST		DESCRIPTION
ITEM	PART NO.	SIZE
1	HV-ACO	110 VAC
2	131-A556-0891-552	110 VAC LINE CUTOFF SWITCH
3	CLU5021	110 VAC 15A 120V SPST
4	B3321-L7	CUTTER HAMMER TOGGLE SWITCH
5	175C	CHIMIE PLASTIC (12V 11K)
6	C-35820	ZINC CAN 2 1/2 x 1/2
7	DP-GW-1	HEYMAN STRAIN RELIEF
8	10-21-5	SOC HD CAP SCR
9	6-57-4	BUTTON HD CAP SCR
10	B-32711D	HEX NUT
11	N# 6	LOCKWASH 1/2
12	757-3PN-059	DEUTSCHE CABLE CONNECTOR
13	1250	ALPHA CABLE
14	C7A(NE20)	NEON LAMP
15	1451	ALPHA CABLE
16	SRGP-4	HEYMAN STRAIN RELIEF



SCHEMATIC

NO. PTP - 1241 PER REV. ASB.
MATERIAL -
FINISH -
MT. THT. -

BOLLER & CHIVENS
SOLVED THE PROBLEMS OF COMMUNICATIONS

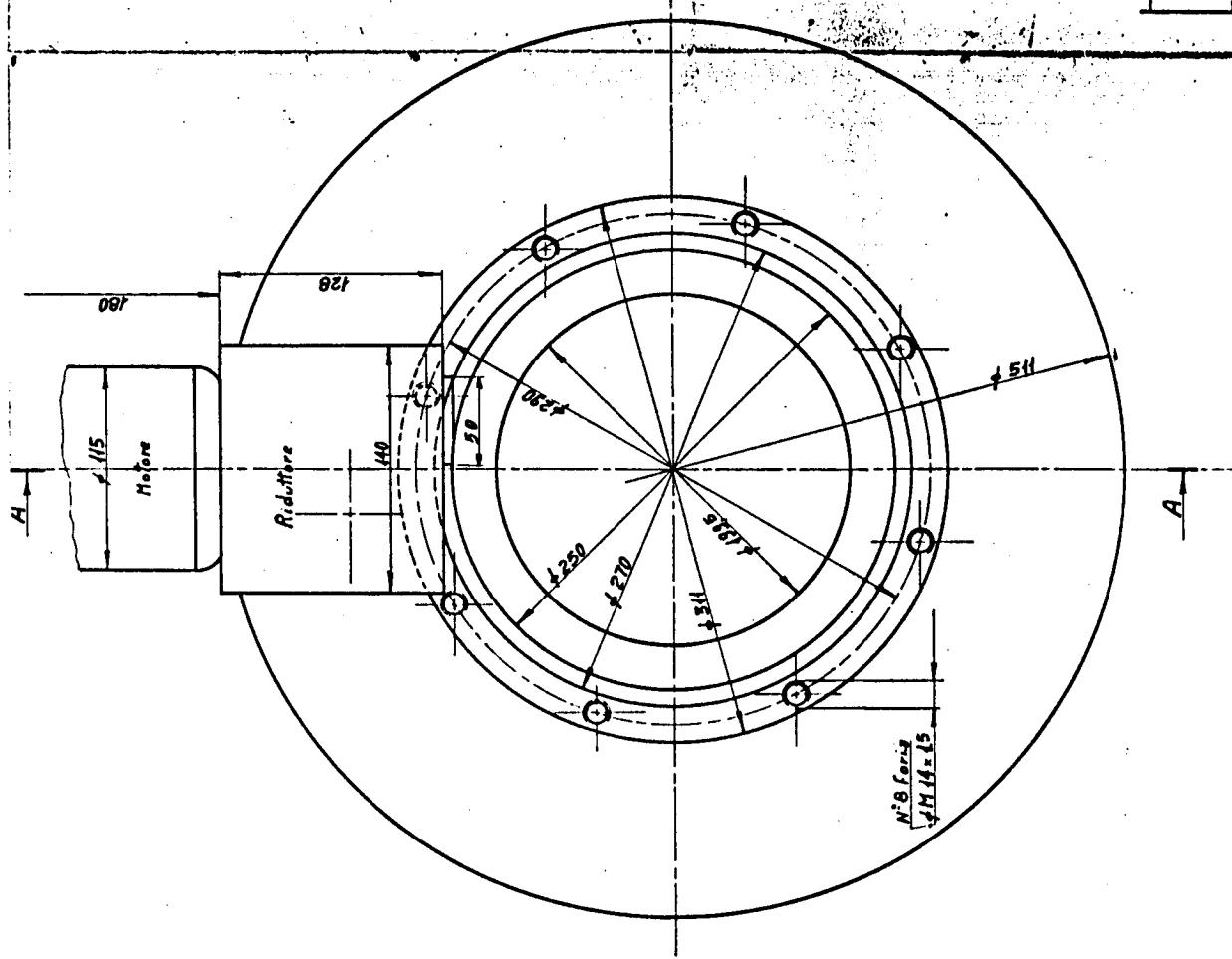
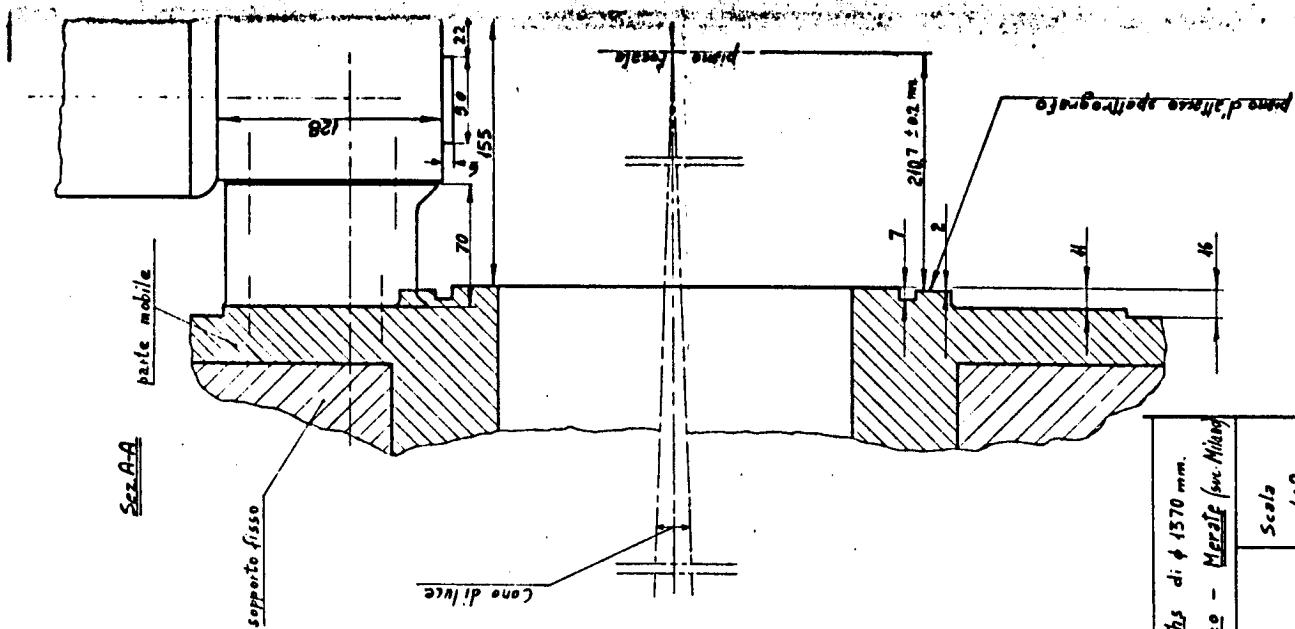
ESTABLISHED 1872
MANUFACTURERS OF TELEGRAPH EQUIPMENT

1241 E-1991 C-35820

E-38922 58771 59007 58614 58407

— NEXT ASB. —
JOB NO. —

1241 E-1991 C-35820



Telescopio Riflettore Ruths di ϕ 1370 mm.	
- Osservatorio Astronomico - Merate (in Milano)	
Diseño:	Flange d'attacco sbarparese
Scala	1:2
Designner:	Carlo S.
Date:	26/11/74

Telescopio Riflettore Ruotis di ϕ 1370 mm. - Osservatorio Astronomico - Milano - (Istituto Meete)	
Object: Adaptive Flange for Spectrograph	Scale 1:2
Date: 23/4/73	Author: A.R.D. Sartori

